

Modification of turbulent friction drag by streamwise-traveling waves of spanwise wall velocity

Pierre Ricco¹, Maurizio Quadrio² & Claudio Viotti²

¹Department of Mechanical Engineering - King's College London
pierre.ricco@kcl.ac.uk - <http://www.pierre-ricco.co.uk>

²Dipartimento di Ingegneria Aerospaziale - Politecnico di Milano
maurizio.quadrio@polimi.it - <http://www.aero.polimi.it/quadrio/>

European Drag Reduction & Flow Control Meeting
Ostritz - St. Marienthal, Germany, 8-11 Sept. 2008

MOTIVATION AND TECHNIQUES

Motivation

- Understanding flow physics
- Flow modification for a better system efficiency

Turbulent friction drag reduction

- **Active** technique
- **Net** energy balance: $P_{net}(\%) = DR(\%) - P_{sp}(\%)$
- Accuracy is key to calculate net balance

Spanwise forcing of near-wall turbulence

- Spanwise wall **oscillation** below wall turbulence - *TIME*
- **Standing** wave of spanwise wall velocity - *SPACE*
- **Traveling** waves of spanwise wall velocity - *SPACE-TIME*

Channel flow: DNS Politecnico di Milano

MOTIVATION AND TECHNIQUES

Motivation

- Understanding flow physics
- Flow modification for a better system efficiency

Turbulent friction drag reduction

- Active technique
- Net energy balance: $P_{net}(\%) = DR(\%) - P_{sp}(\%)$
- Accuracy is key to calculate net balance

Spanwise forcing of near-wall turbulence

- Spanwise wall oscillation below wall turbulence - TIME
- Standing wave of spanwise wall velocity - SPACE
- Traveling waves of spanwise wall velocity - SPACE-TIME

Channel flow: DNS Politecnico di Milano

MOTIVATION AND TECHNIQUES

Motivation

- Understanding flow physics
- Flow modification for a better system efficiency

Turbulent friction drag reduction

- **Active** technique
- **Net** energy balance: $P_{net}(\%) = DR(\%) - P_{sp}(\%)$
- Accuracy is key to calculate net balance

Spanwise forcing of near-wall turbulence

- Spanwise wall **oscillation** below wall turbulence - *TIME*
- **Standing** wave of spanwise wall velocity - *SPACE*
- **Traveling** waves of spanwise wall velocity - *SPACE-TIME*

Channel flow: DNS Politecnico di Milano

MOTIVATION AND TECHNIQUES

Motivation

- Understanding flow physics
- Flow modification for a better system efficiency

Turbulent friction drag reduction

- **Active** technique
- **Net** energy balance: $P_{net}(\%) = DR(\%) - P_{sp}(\%)$
- Accuracy is key to calculate net balance

Spanwise forcing of near-wall turbulence

- Spanwise wall **oscillation** below wall turbulence - *TIME*
- **Standing** wave of spanwise wall velocity - *SPACE*
- **Traveling** waves of spanwise wall velocity - *SPACE-TIME*

Channel flow: DNS Politecnico di Milano

TURBULENT DRAG REDUCTION

Spanwise wall oscillations

$$W = W_m \sin(2\pi t/T)$$

- W_m maximum wall velocity - T period of oscillation

Standing wave of spanwise wall velocity

$$W = W_m \sin(2\pi x/\lambda_x)$$

- λ_x streamwise wavelength

Streamwise-traveling waves of spanwise wall velocity

$$W = W_m \sin(\kappa_x x - \omega t)$$

- $\kappa_x = 2\pi/\lambda_x$ - $\omega = 2\pi/T$



TURBULENT DRAG REDUCTION

Spanwise wall oscillations

$$W = W_m \sin(2\pi t/T)$$

- W_m maximum wall velocity - T period of oscillation

Standing wave of spanwise wall velocity

$$W = W_m \sin(2\pi x/\lambda_x)$$

- λ_x streamwise wavelength

Streamwise-traveling waves of spanwise wall velocity

$$W = W_m \sin(\kappa_x x - \omega t)$$

- $\kappa_x = 2\pi/\lambda_x$ - $\omega = 2\pi/T$



TURBULENT DRAG REDUCTION

Spanwise wall oscillations

$$W = W_m \sin(2\pi t/T)$$

- W_m maximum wall velocity - T period of oscillation

Standing wave of spanwise wall velocity

$$W = W_m \sin(2\pi x/\lambda_x)$$

- λ_x streamwise wavelength

Streamwise-traveling waves of spanwise wall velocity

$$W = W_m \sin(\kappa_x x - \omega t)$$

- $\kappa_x = 2\pi/\lambda_x$ - $\omega = 2\pi/T$



TURBULENT DRAG REDUCTION

Spanwise wall oscillations

$$W = W_m \sin(2\pi t/T)$$

- W_m maximum wall velocity - T period of oscillation

Standing wave of spanwise wall velocity

$$W = W_m \sin(2\pi x/\lambda_x)$$

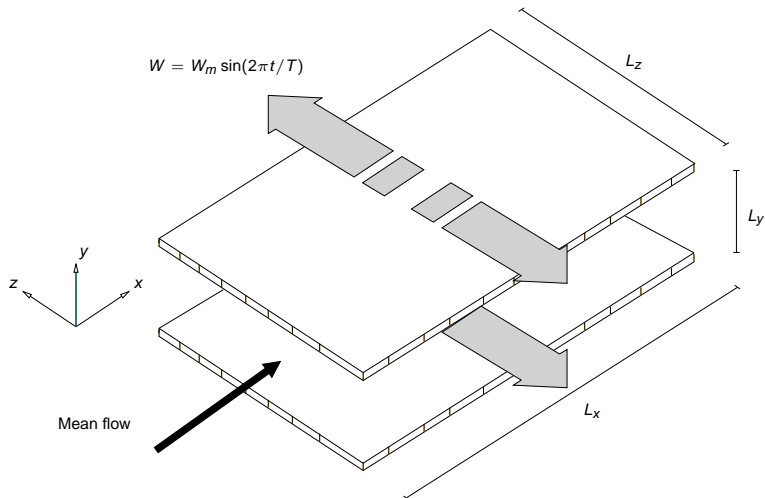
- λ_x streamwise wavelength

Streamwise-traveling waves of spanwise wall velocity

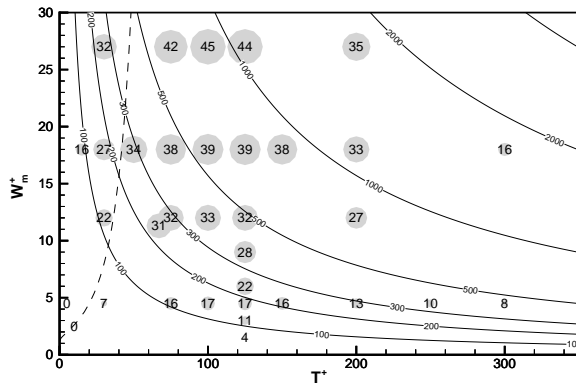
$$W = W_m \sin(\kappa_x x - \omega t)$$

- $\kappa_x = 2\pi/\lambda_x$ - $\omega = 2\pi/T$

THE OSCILLATING-WALL FLOW

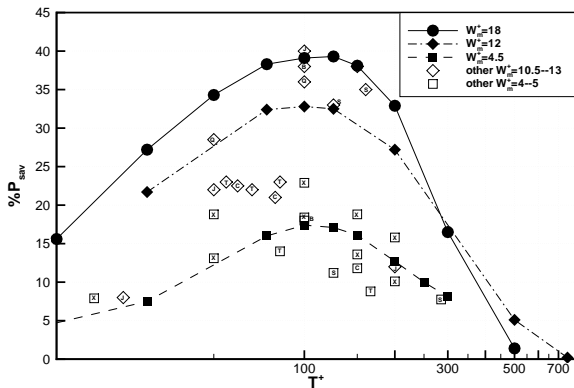


MAP OF DRAG REDUCTION



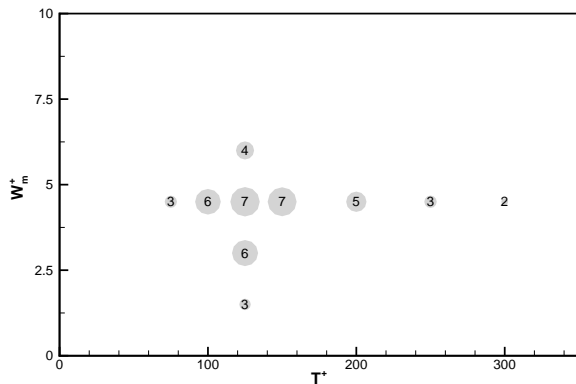
- $DR\%$ as function of W_m and T
- Optimal frequency - $DR\%$ grows with W_m

OPTIMAL FREQUENCY



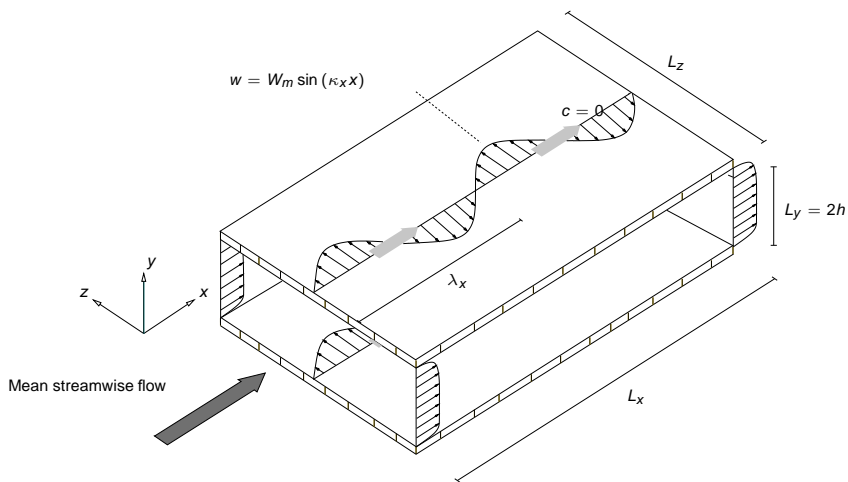
- Optimal frequency at fixed W_m
- It does not depend on W_m

MAP OF NET ENERGY SAVING

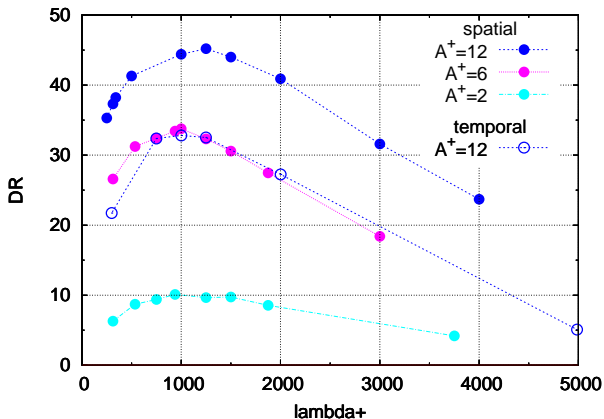


- Net energy balance: $P_{net}(\%) = DR(\%) - P_{sp}(\%)$
- Optimal T - Optimal W_m - unsteady \rightarrow NOT practical

THE STANDING-WAVE FLOW

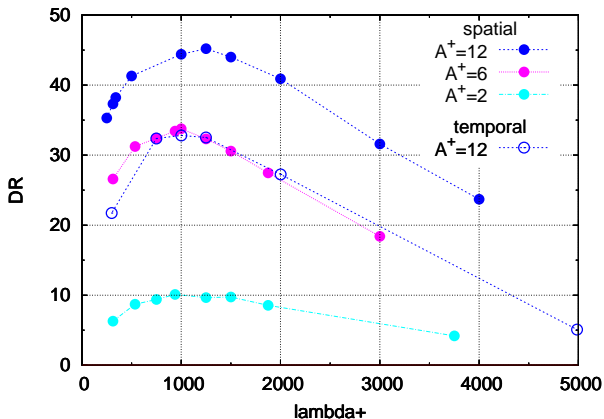


OPTIMAL WAVELENGTH



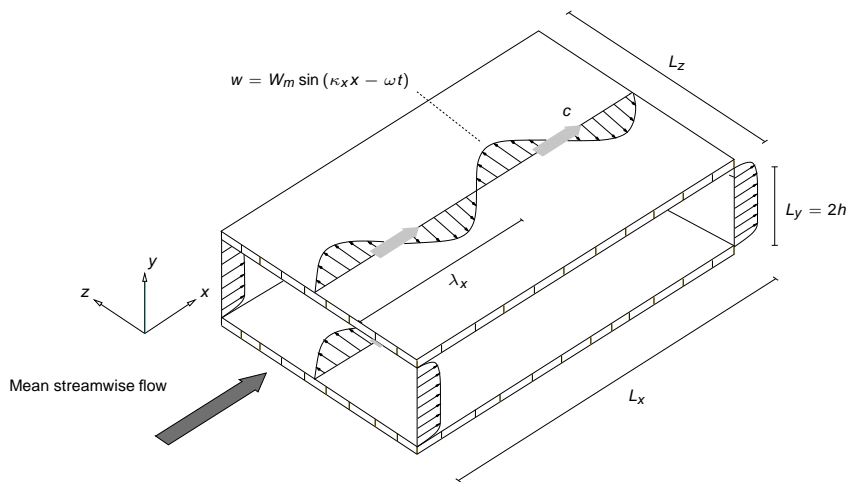
- Optimal wavelength - U_w convection velocity
- $U_w = \lambda_{x,opt}/T_{opt}$ - steady \rightarrow roughness?

OPTIMAL WAVELENGTH

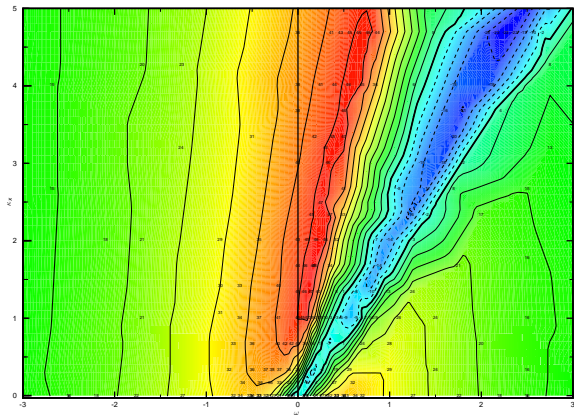


- **Optimal wavelength - U_w convection velocity**
- $U_w = \lambda_{x,opt}/T_{opt}$ - steady \rightarrow roughness?

THE TRAVELING-WAVE FLOW

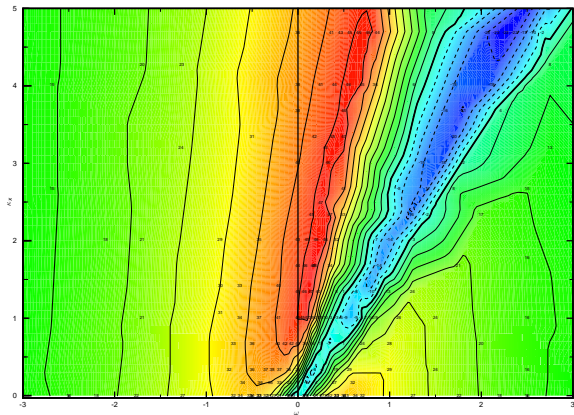


MAP OF DRAG MODIFICATION - $W_m^+ = 12$



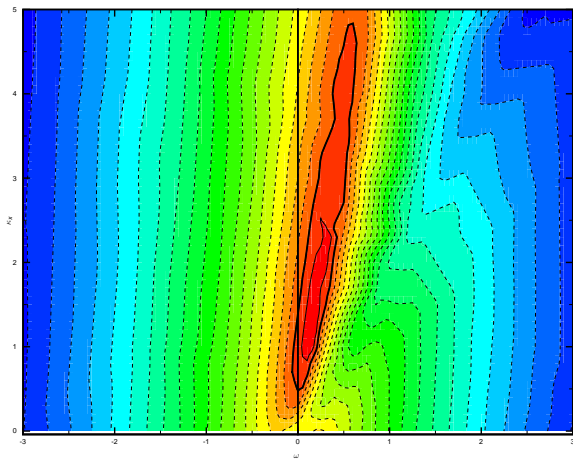
- Blue: *Drag increase* $\sim 20\%$ - $c \approx U_w$
- Red: *Drag reduction* $\sim 45\%$

MAP OF DRAG MODIFICATION - $W_m^+ = 12$



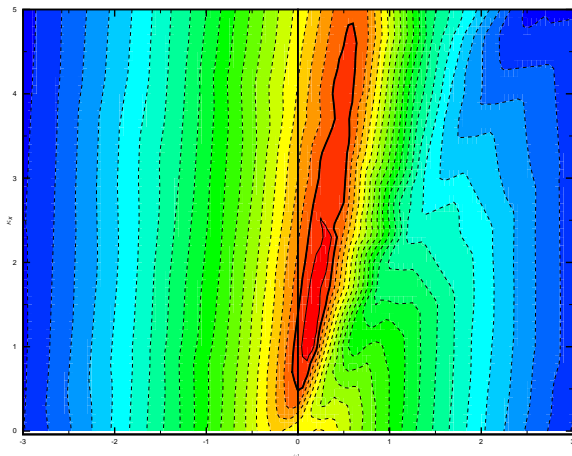
- Blue: **Drag increase** $\sim 20\%$ - $c \approx U_w$
- Red: **Drag reduction** $\sim 45\%$

MAP OF NET ENERGY SAVING - $W_m^+ = 12$



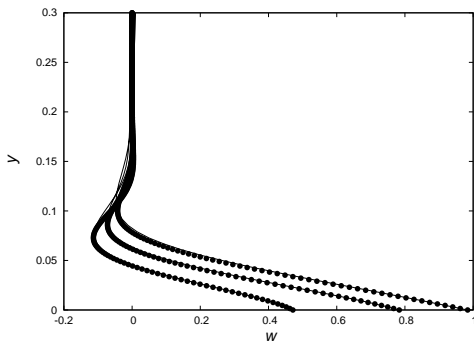
- Red-thick line - **Positive net balance: $MAX \approx 18\%$**
- Oscillating wall give *negative* balance at this W_m^+

MAP OF NET ENERGY SAVING - $W_m^+ = 12$



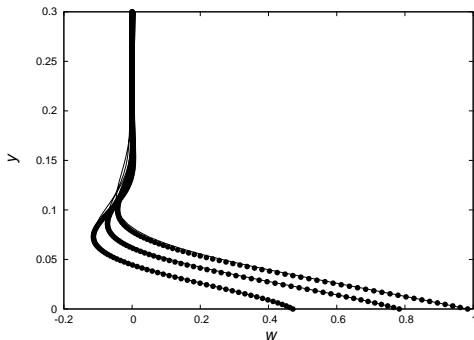
- Red-thick line - **Positive net balance: $MAX \approx 18\%$**
- Oscillating wall give *negative* balance at this W_m^+

TURBULENT AND LAMINAR SPANWISE FLOW



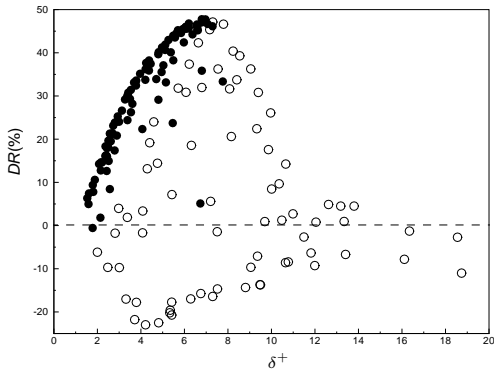
- $w = W_m \Re \left\{ C e^{2\pi i(x-ct)/\lambda_x} \text{Ai} \left[e^{\pi i/6} (2\pi\tau^*/(\lambda_x\nu))^{1/3} (y - c/u_\tau) \right] \right\}$
- Good agreement despite simplifications small δ - long λ_x
- Major advantage for further analysis DR scaling

TURBULENT AND LAMINAR SPANWISE FLOW



- $w = W_m \Re \left\{ C e^{2\pi i(x-ct)/\lambda_x} \text{Ai} \left[e^{\pi i/6} (2\pi\tau^*/(\lambda_x\nu))^{1/3} (y - c/u_\tau) \right] \right\}$
- Good agreement despite simplifications small δ - long λ_x
- Major advantage for further analysis DR scaling

GENERALIZED STOKES LAYER THICKNESS



$$\mathcal{T} \equiv \frac{\lambda_x}{U_w - c} = \frac{2\pi}{U_w \kappa_x - \omega}$$

Equivalent period of forcing - MINIMAL CONDITIONS $\delta^+ \approx 1$

SUMMARY AND FUTURE WORK

Summary

- **Oscillating wall**: nice, instructive, **not** practical
- **Standing wave**: **steady** - roughness?
- **Traveling wave**: highly efficient!

Future work

- Physics: near-wall turbulence
- Scaling of drag modification
- Experiments on traveling waves!