

Skin-friction drag reduction via steady streamwise oscillations of spanwise velocity

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Skin friction drag-reduction

Spanwise-based methods

Obivious requirements

- Simple \Rightarrow feasible
- Energy efficient \Rightarrow net saving

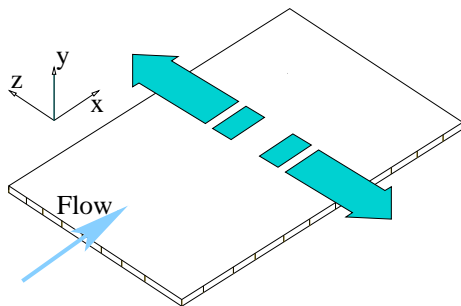
Additional requirement

- **Steady** \Rightarrow convertible into **passive** device ??

Temporal-oscillating wall

Jung, Mangiavacchi & Akhavan (PoF, 1992)

$$W_w = A \sin\left(\frac{2\pi}{T} t\right)$$



- Stokes layer interacts with wall structures
- DR up to 40%
- optimal period $T_{opt}^+ \approx 100 - 125$
- net energy saving up to 7%
- **unsteady!!**

Spanwise forcing

Further studies and variants

W_w

$$A \sin\left(\frac{2\pi}{T} t\right)$$

Temporal-oscillating wall

Jung *et al.* (1992), Laadhari *et al.* (1994),
J. I. Choi *et al.* (2002), Quadrio & Ricco (2003, 2004)

$$A \sin\left(\frac{2\pi}{\lambda} z - \frac{2\pi}{T} t\right)$$

Zhao *et al.* (2004)

F_z

$$A e^{-y/\Delta} \sin\left(\frac{2\pi}{T} t\right)$$

Spanwise body force

Du *et al.* (2002), Berger *et al.* (2000),
Breuer *et al.* (2004)

$$A e^{-y/\Delta} \sin\left(\frac{2\pi}{\lambda} z\right)$$

Du *et al.* (2002)

$$A e^{-y/\Delta} \sin\left(\frac{2\pi}{\lambda} z - \frac{2\pi}{T} t\right)$$

Du *et al.* (2002), Zhao *et al.* (2004),
Pang & K.S. Choi (2004)

$$A e^{-y/\Delta} \sin\left(\frac{2\pi}{\lambda} x\right)$$

Berger *et al.* (2000)

Question

Can a **temporal** oscillation be converted into a **spatial** oscillation?

Possible answer

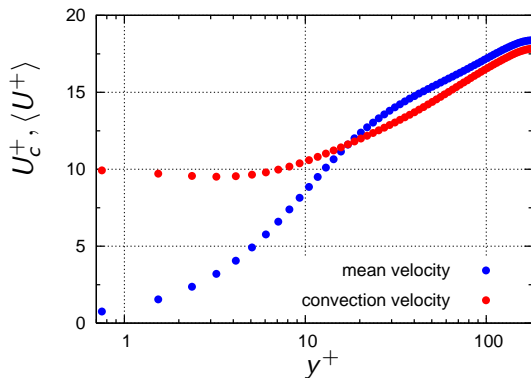
Yes, by exploiting the **convective nature** of the flow

Convection velocity in turbulent wall flows

Quadrio & Luchini, Pof 2003

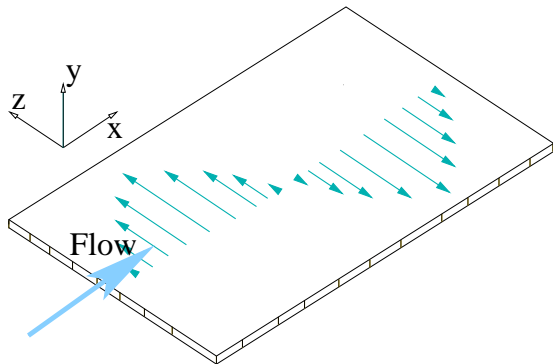
Channel flow,
DNS at $Re_\tau = 180$

- convection velocity of turbulent fluctuations
- convection is not zero at the wall!
- near wall: $U_c^+ \approx 10$



Our control law: streamwise steady waves

$$W_w = A \sin\left(\frac{2\pi}{\lambda_x} x\right)$$



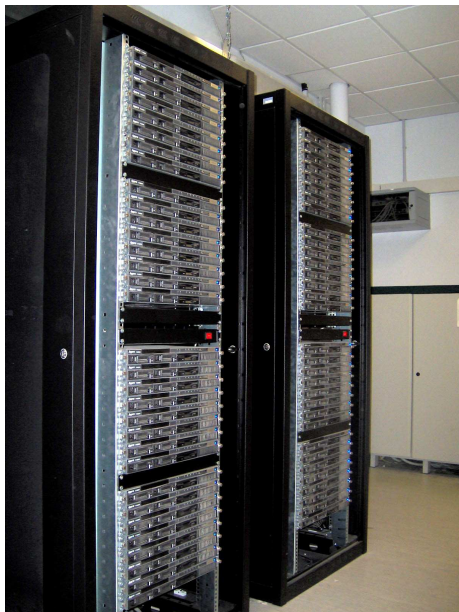
TWO PARAMETERS

- Amplitude A
- Wavelength λ_x

- Turbulent channel flow at $Re_\tau = 200$
- Domain size: $L_x = 6\pi h$, $L_y = 2h$, $L_z = 3\pi h$
- Spatial resolution: $N_x \times N_y \times N_z = 320 \times 160 \times 320$
- Averaging time: 10^4 viscous time units
- **Number of simulations: 35**

Computing tool

- DNS pseudo-spectral code
- Parallel computing on commodity hardware (Luchini & Quadrio JCP-2006)
- The “Personal Supercomputer”:
Powerful **dedicated** system with
128 Opteron CPUs, 100GB
RAM, 4TB disk

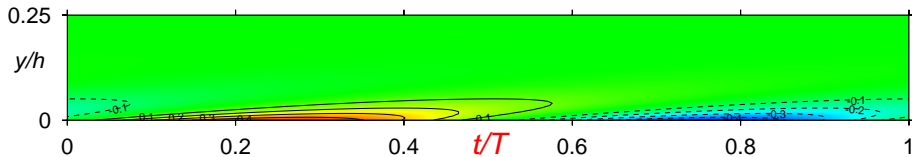


Spanwise flow (1)

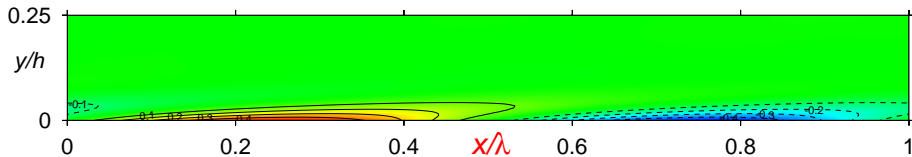
The laminar case

Contour of spanwise velocity W

Temporal oscillation



Spatial oscillation



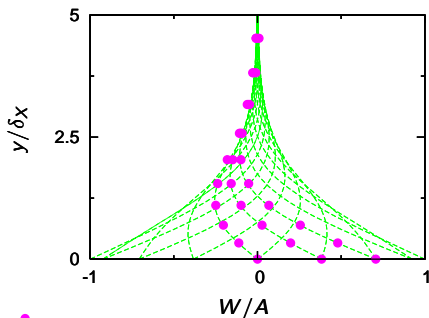
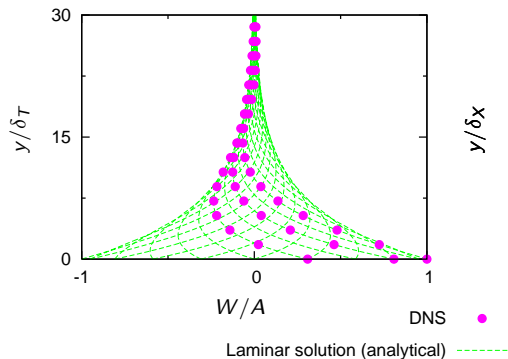
Spanwise flow (2)

Laminar solution vs. turbulent DNS data

$$\delta_T = \nu^{1/2} T^{1/2}$$

$$\delta_X = \nu^{1/3} \lambda_x^{1/3} \frac{dU}{dy}^{-1/3}$$

► details



Spanwise-averaged turbulent flow coincides with analytical solution in both cases

A natural question

TEMPORAL
OSCILLATION

$$T_{opt}^+ \approx 100 - 125$$

$$U_c^+ = 10$$



SPATIAL
OSCILLATION

$$\lambda_{opt}^+ \approx 1000 - 1250 ??$$

A natural question

TEMPORAL
OSCILLATION

$$T_{opt}^+ \approx 100 - 125$$

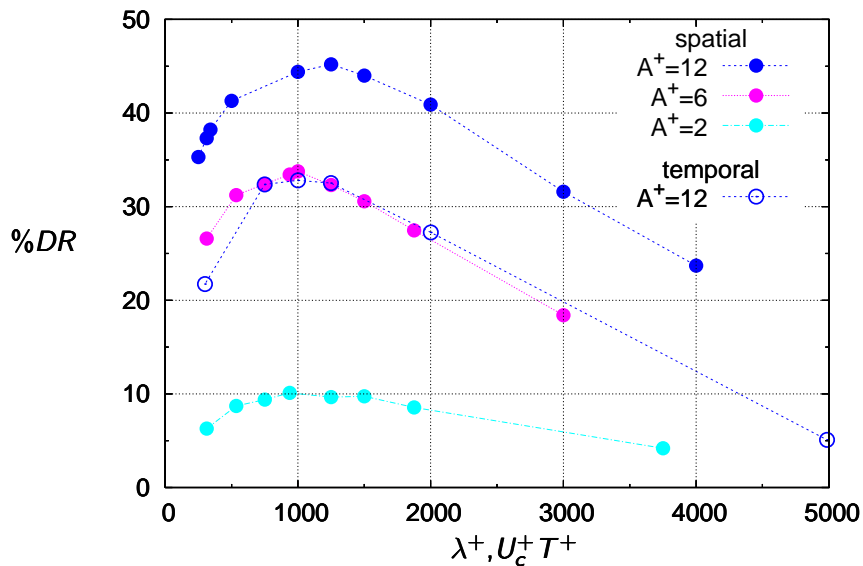
$$U_c^+ = 10$$



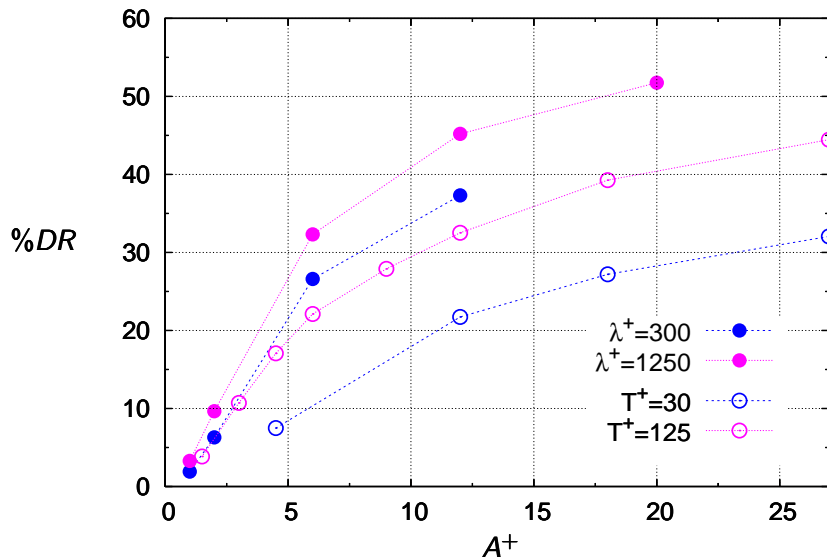
SPATIAL
OSCILLATION

$$\lambda_{opt}^+ \approx 1000 - 1250 ??$$

Drag reduction (1)



Drag reduction (2)



Power budget: definitions

- Power required to **drive** the flow:

$$P_{drive} = \mu \left\langle \frac{\partial U}{\partial y} \frac{Q_x}{h} \right\rangle$$

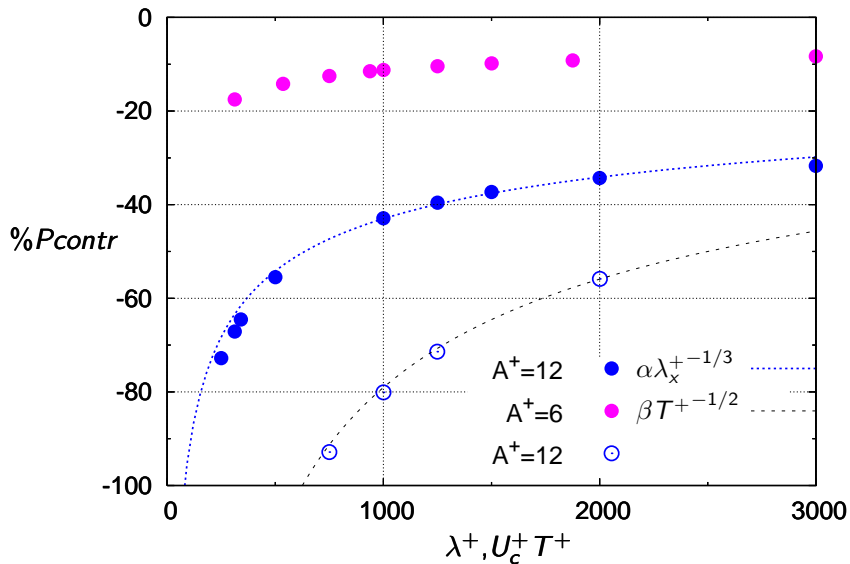
- Power required to **control** the flow:

$$P_{contr} = \mu \left\langle \frac{\partial W}{\partial y} W \right\rangle$$

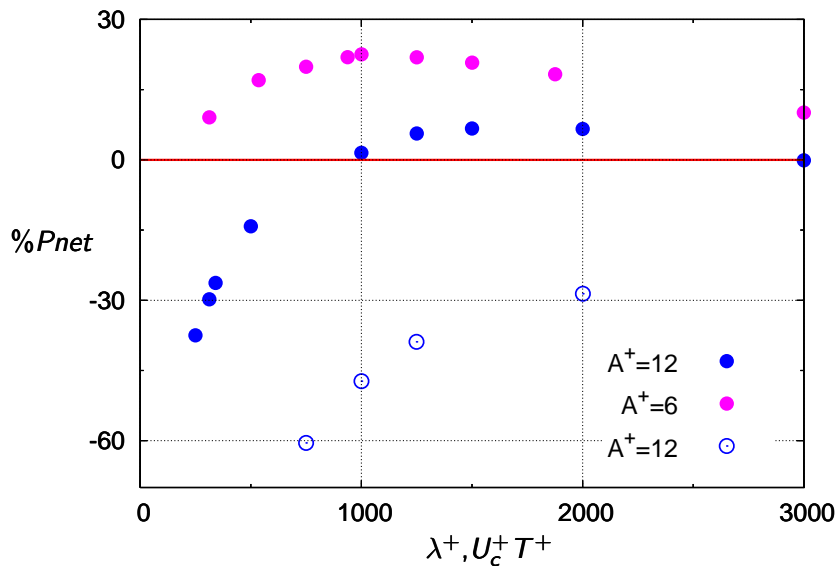
- **Net** power saved after DR:

$$P_{net} = \Delta P_{drive} + P_{contr}$$

Power budget (1)

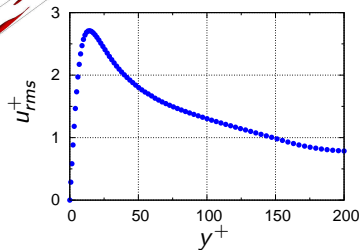
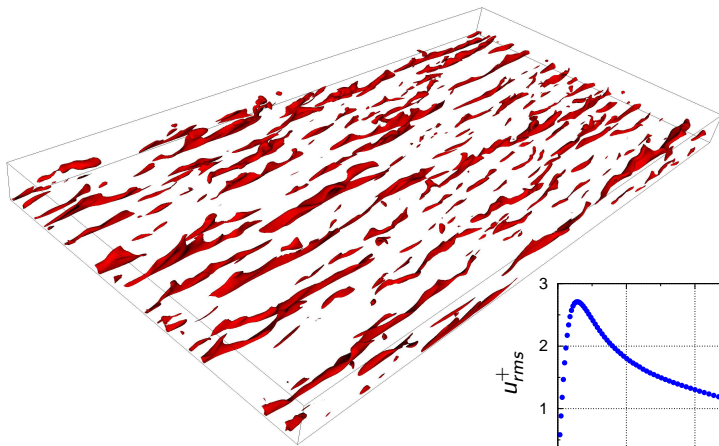


Power budget (2)



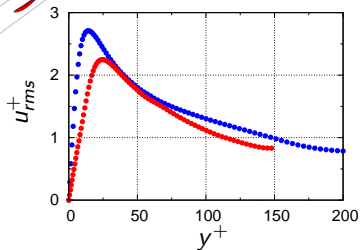
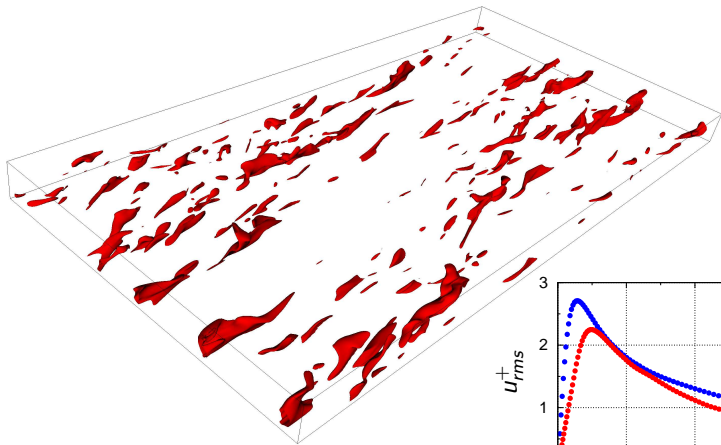
Isosurfaces of streamwise velocity: $u^+ = -4$

Uncontrolled

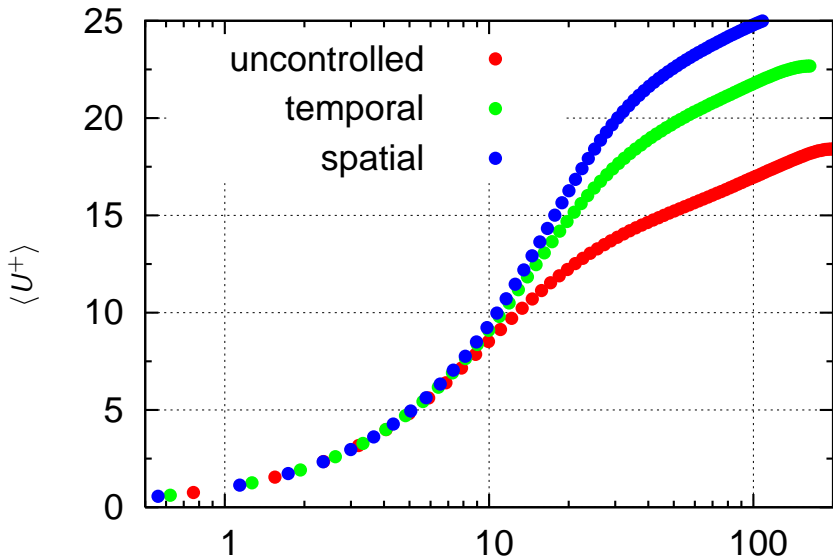


Isosurfaces of streamwise velocity: $u^+ = -4$

Controlled, *DR* 45%, **actual wall units**



Mean velocity profiles



- 1 U_c translates temporal into spatial forcing
- 2 Spatial forcing is more efficient
 - Higher DR (up to 52%)
 - Higher net saving (up to 23%)
- 3 Turbulent spanwise mean flow is based on laminar dynamics
 - Passive device?

Spanwise flow (3)

Spatial oscillation - analytical results

Governing equation for z-component of velocity

$$U(y) \frac{\partial W}{\partial x} = \nu \left(\frac{\partial^2 W}{\partial x^2} + \frac{\partial^2 W}{\partial y^2} \right)$$

Hypothesis (δ_x thickness of the “spatial Stokes layer”)

$$\delta_x \ll h, \quad \lambda = \mathcal{O}[h] \quad \Rightarrow \quad \frac{\partial^2 W}{\partial x^2} \ll \frac{\partial^2 W}{\partial y^2}, \quad U(y) \sim \left. \frac{dU}{dy} \right|_w y$$

Simplified governing equation:

$$\left. \frac{dU}{dy} \right|_w y \frac{\partial W}{\partial x} = \nu \frac{\partial^2 W}{\partial y^2}$$

Spanwise flow (4)

Spatial oscillation - analytical results

It is possible to look for a solution in the form

$$W(x, y) = \Re \left[e^{i2\pi/\lambda x} F(y) \right]$$

obtaining a complex **Airy equation** for $F(y)$

$$i \frac{dU}{dy} \Big|_w y F(y) = \nu \lambda \frac{d^2 F(y)}{dy^2}$$

$$\xRightarrow{\text{solution}} F(y) = C \mathcal{A} \left(e^{-i2\pi/3} i \frac{y}{\nu^{1/3} \lambda^{1/3} \frac{dU}{dy} \Big|_w^{-1/3}} \right)$$

$$\delta_X = \nu^{1/3} \lambda_x^{1/3} \frac{dU}{dy} \Big|_w^{-1/3}$$