



## Theoretical and Experimental Investigation of Aeroelastic Rotorcraft-Pilot Coupling

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- Aeroelastic Rotorcraft/Pilot Couplings
- Investigation Description
- Simplified Aeroelastic Model
- Experimental Activity
- Discussion of Results
- Conclusions

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Aircraft/Rotorcraft-Pilot Couplings are

*“unintentional (inadvertent) sustained or uncontrollable vehicle oscillation characterized by a mismatch between the pilot’s mental model of the vehicle dynamics and the actual vehicle dynamics.” (Mc Ruer)*

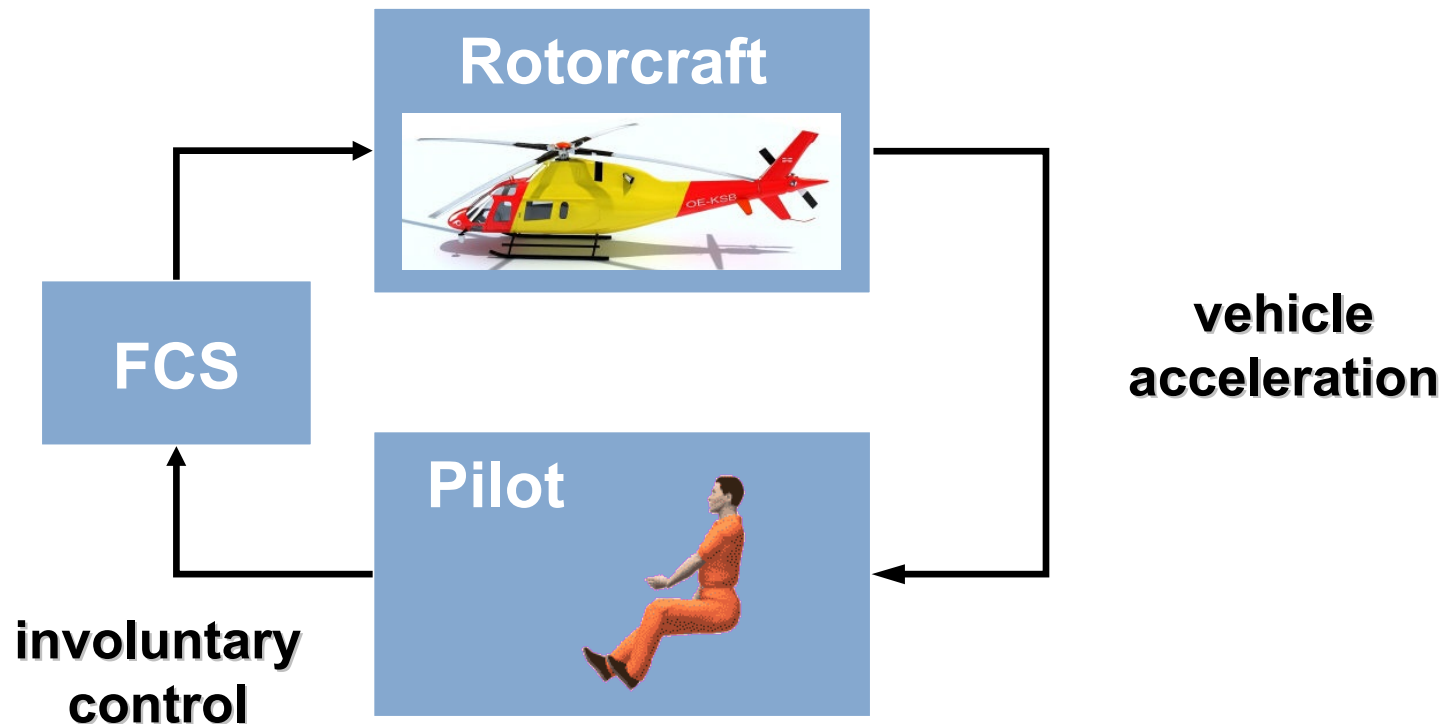
ARISTOTEL: research project sponsored by EC 7th FP led by TUDelft

*Aircraft and Rotorcraft Pilot Couplings Tools  
and Techniques for Alleviation and Detection*  
<http://www.aristotelproject.eu/>



This presentation is related to experimental research on aeroelastic RPC resulting from involuntary control inputs generated by the pilot as a consequence of vibrations of the vehicle in pilot-in-the-loop conditions.

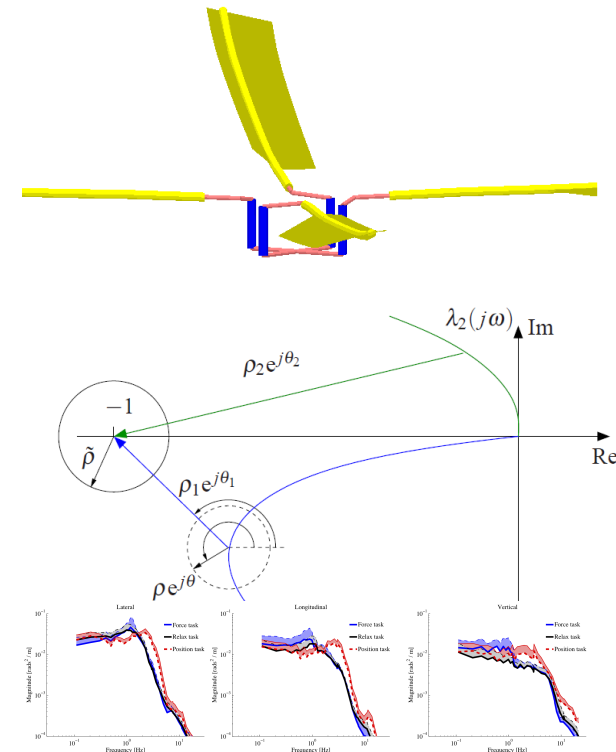
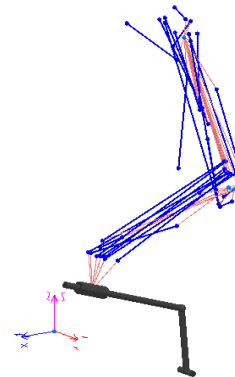
- **Voluntary interaction (PIO)** “active” pilot intervention
- **Involuntary interaction (PAO)** “passive” pilot intervention (biodynamic feedthrough)



Within ARISTOTEL, aeroelastic RPCs:

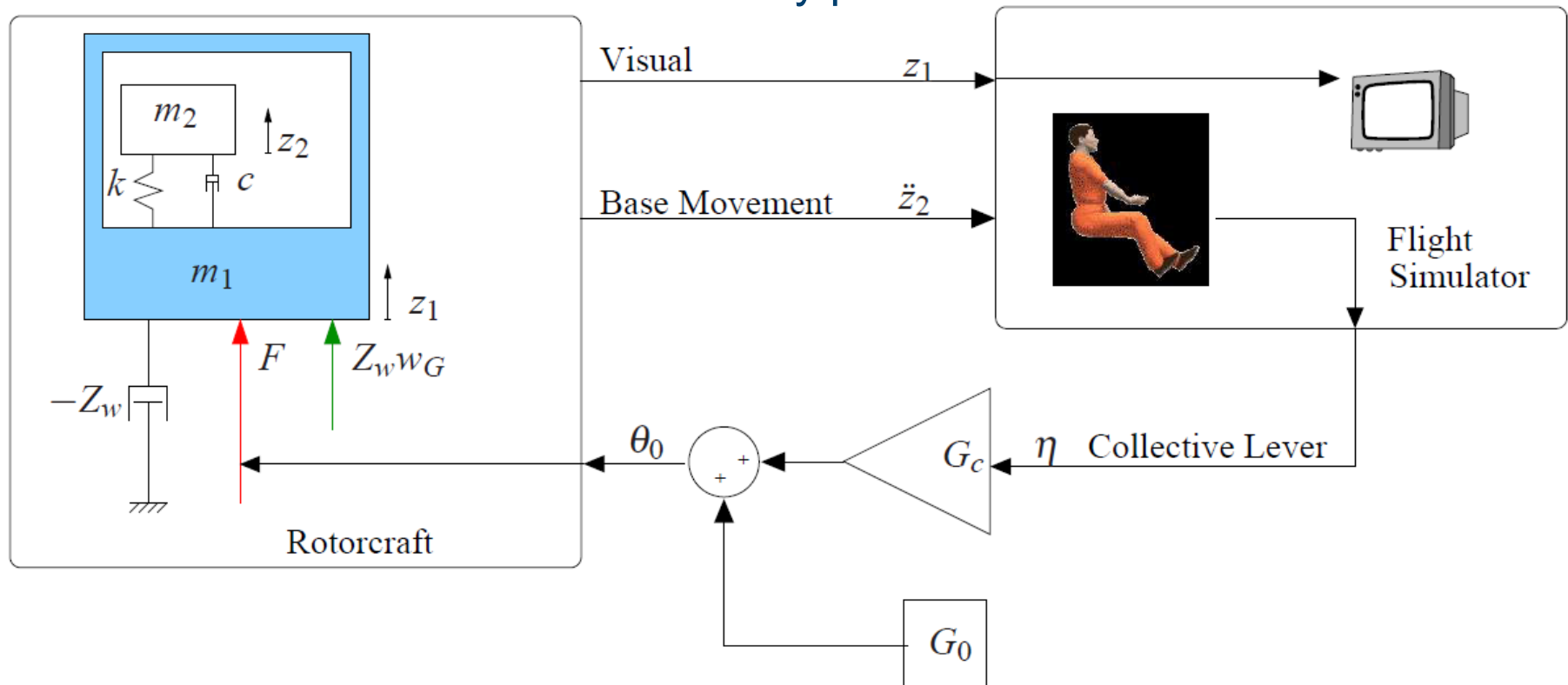
- POLIMI working on
  - Vehicle modeling & fidelity requirements
  - Pilot biomechanics: detailed biom. models
  - Tools for prediction and means for prevention (robust stability)
- UoL working on
  - Flight simulation of aeroelastic rotorcraft
  - Experimental investigation of pilot BDFT

All activities in strict cooperation with the other partners.



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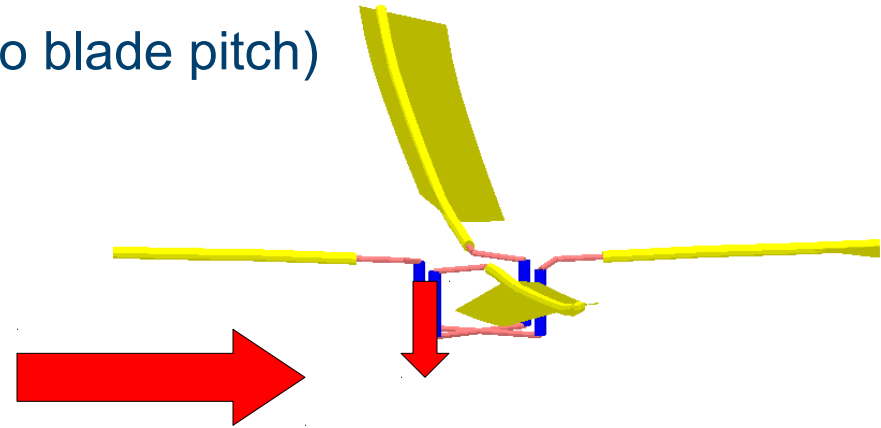
- Implement simple “aeroelastic” flight mechanics model in flight sim.
  - restricted to **heave only**, with **elastic** degree of freedom
- Test with pilot-in-the-loop, to:
  - trigger bioaeroelastic instabilities
  - understand how the human operator interacts with true feedback
  - determine the influence of key parameters





Investigated parameters include:

- stiffness and damping of elastic mode
- gearing ratio  $G_c$  (collective lever to blade pitch)



- presence/absence of (emulated) friction in collective control lever
- task

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- Heave degree of freedom only

$$m_t \dot{w} = Z$$

- Aerodynamics linearized about hover condition

$$Z = Z_w (w - w_G) + Z_{\theta_0} \theta$$

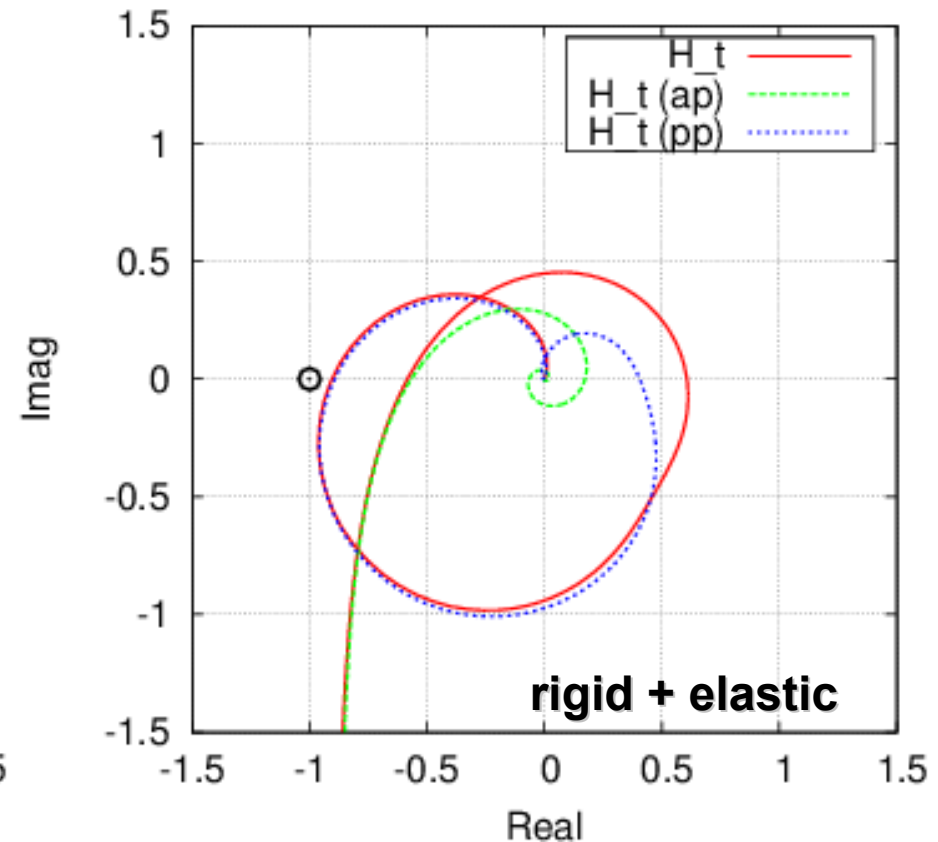
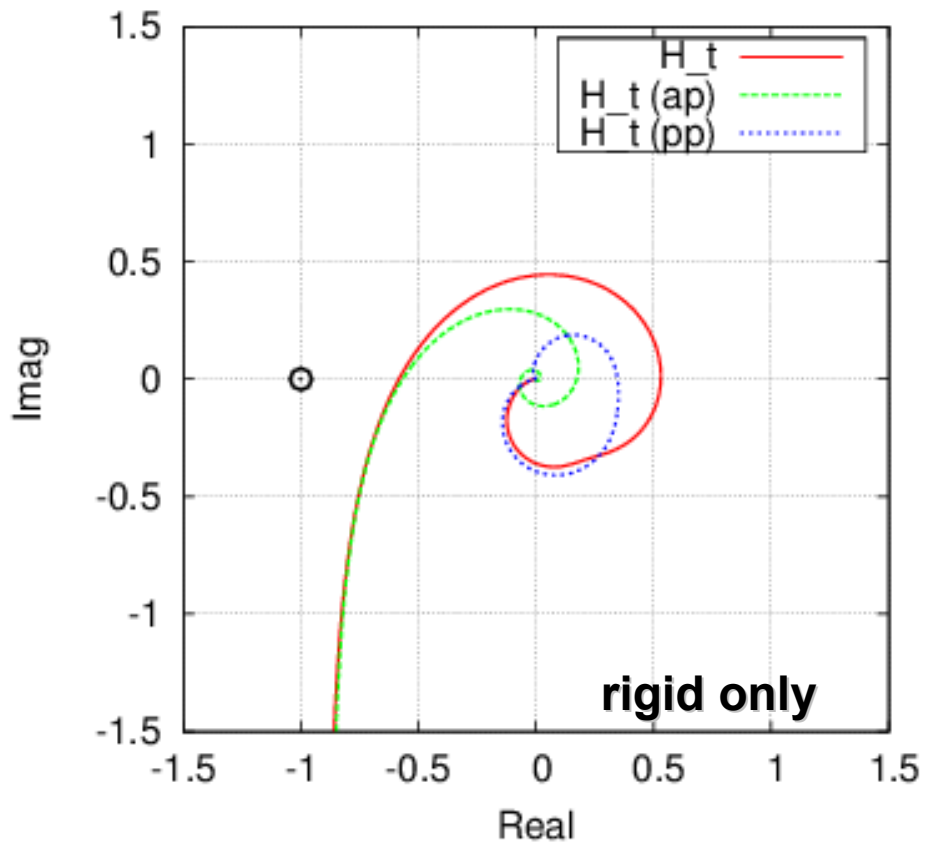
- Motion of pilot's seat associated with “elastic” degree of freedom

$$m_t \ddot{z}_1 - Z_w \dot{z}_1 = Z_{\theta_0} \theta - Z_w w_G$$

$$m_2 \ddot{z}_2 + c \dot{z}_2 + k z_2 = c \dot{z}_1 + k z_1$$

- “rigid” helicopter degree of freedom associated with visual demand
- “elastic” DOF associated with flight simulator motion demand
- collective control resulting from control inceptor (pilot-in-the-loop)
- gust velocity used to “disturb” the simulation

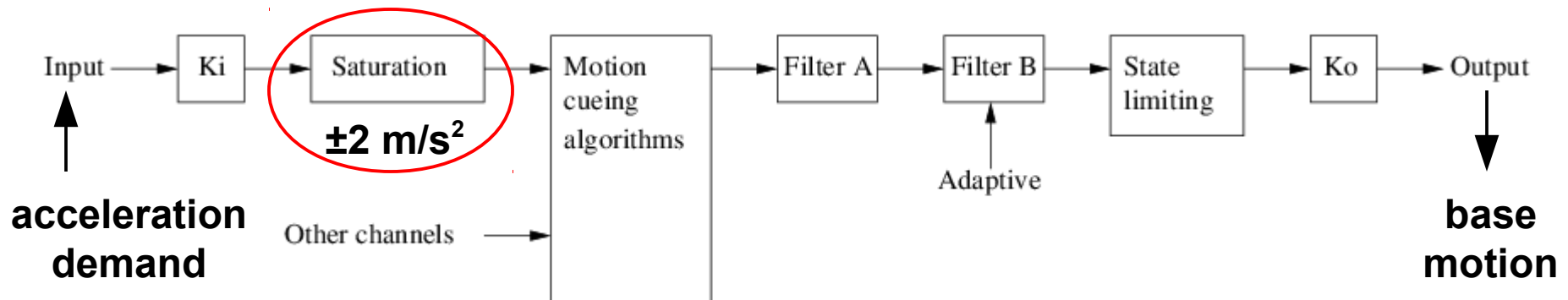
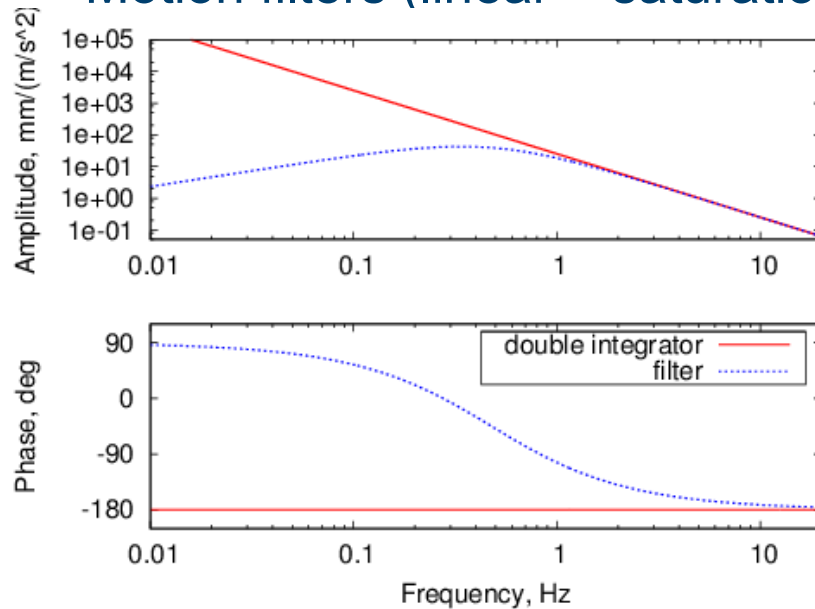
- Nyquist plot of loop TF (data representative of SA 330 Puma):
  - “active” pilot (Mc Ruer's “crossover” model + low-pass filter)
  - BDFT (Mayo's function adapted to UoL's cockpit layout + h.p.f.)
- Elastic mode tuned for marginal stability at about 3.5 Hz (as of BDFT)



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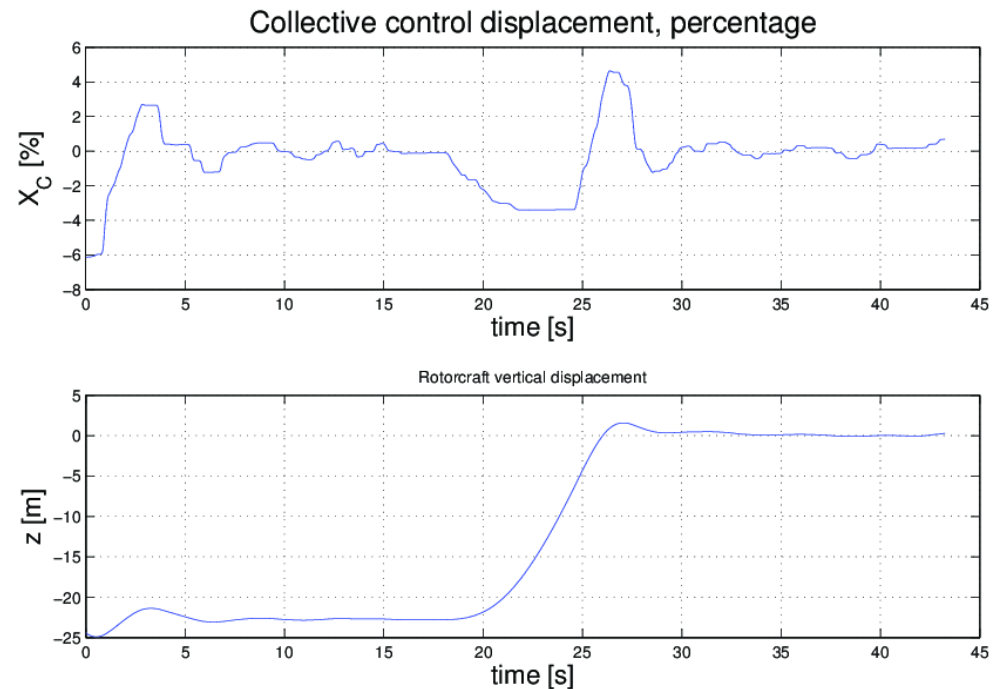
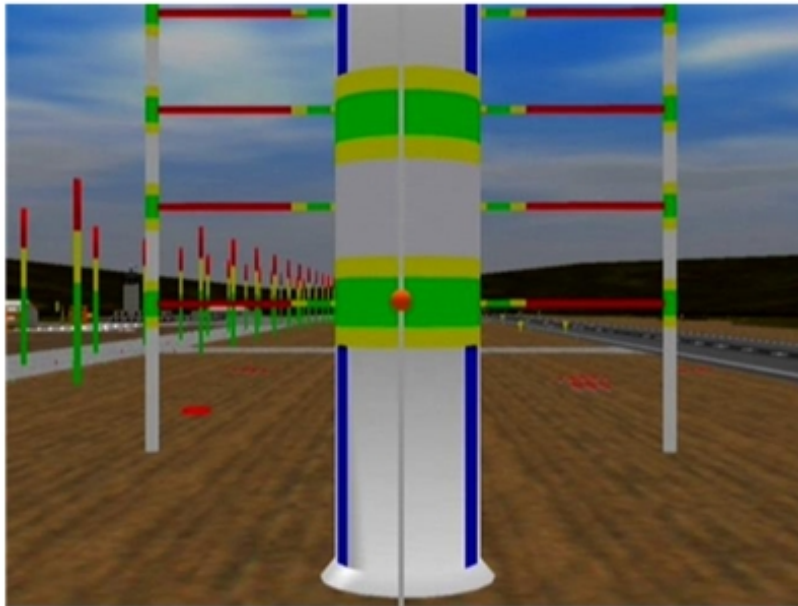
## HELIFLIGHT simulation facility at The University of Liverpool

### Motion filters (linear + saturation)



## Vertical maneuver (ADS-33)

- Primary task: keep the red ball in the green band
- Secondary task: move to a different level (50 ft) when told (workload, trigger)
- Disturbance: oscillatory force with variable frequency and amplitude
- Visual: driven by “rigid body” state
- Motion: driven by “elastic” state



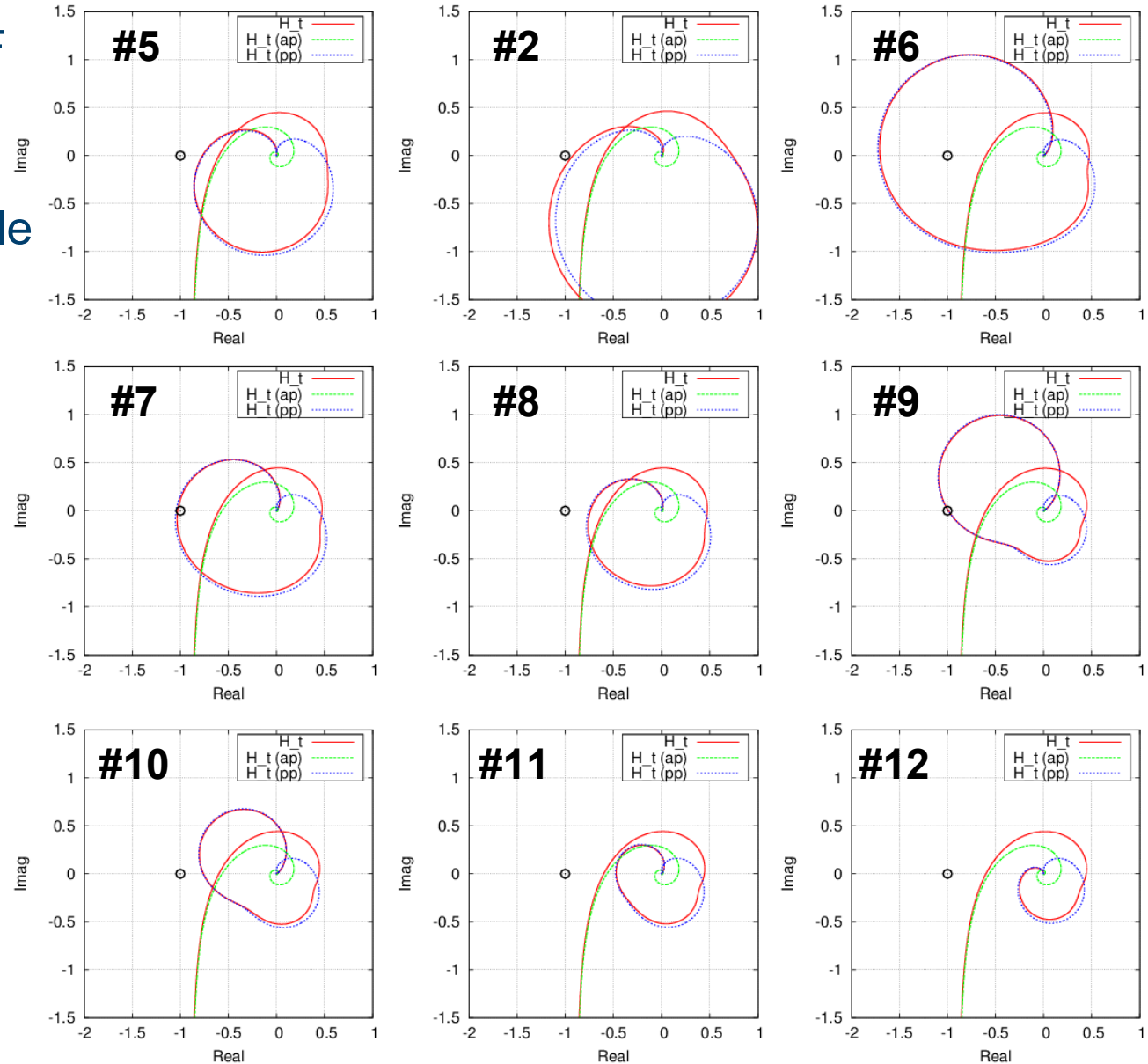
- Tested configurations
  - most planned
  - some designed to better understand incoming results

	#	Pilot	$k/k_{\text{ref}}$	$c/c_{\text{ref}}$	friction	freq. Hz	damp. %
	1	2	0.50	0.15	on	2.53	4.29
	2	1,2,3,4	0.50	0.40	off	2.51	11.41
	3	2	1.00	0.10	on	3.58	2.02
	4	1	1.00	0.20	on	3.57	4.04
<b>nominal</b> →	5	1,2,3,4	1.00	1.00	off,on	3.50	20.15
	6	1,2	1.60	0.40	off	4.51	6.38
	7	2,3	1.60	0.70	off	4.50	11.15
	8	1,2	1.60	1.00	off	4.47	15.93
	9	2	2.80	0.35	off	5.98	4.22
	10	1,2,3	2.80	0.50	off	5.97	6.02
	11	1	2.80	1.00	off	5.94	12.04
	12	1,2,3	3.00	3.00	off,on	5.80	34.89



Predicted loop TF  
of tested cases

Nominally unstable  
ones generated  
during tests while  
looking for LCO



## Test procedure:

- “pilot” (occupant) required to perform primary task (maintain altitude)
- “pilot” (occupant) occasionally instructed to perform secondary task (change altitude)
- disturbance force applied with arbitrary amplitude and frequency
- gearing ratio  $G_c$  modified without informing occupant
- increasingly high levels of  $G_c$  tested until LCO appears (and higher)
  - *safety: motion base saturation, control release procedure*
- 4 occupants: only one professional pilot (former helicopter test pilot)

*task does not require specific piloting skills*

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- Gearing ratio of LCO first appearance and corresponding frequency
- Nominal  $G_c$  is about 0.35 radian

$k/k_{\text{ref}}$	$c/c_{\text{ref}}$	Pilot #1		Pilot #2		Pilot #3		Pilot #4	
		freq., Hz	$G_c$ , radian	freq., Hz	$G_c$ , radian	freq., Hz	$G_c$ , radian	freq., Hz	$G_c$ , radian
Friction off									
3.0	3.0	3.95	$\infty^a$	3.8–4.0	$\infty$	3.9–4.3	$\infty$		
1.0	1.0	3.47	0.7	3.0	0.6	3.2	1.1	2.8	2.5
1.6	1.0	3.93	0.8	3.3	$\infty$				
0.5	0.4	2.56	0.7	2.41	0.4–0.6	2.45	0.7	2.63	0.1
1.6	0.4	3.98	0.4	3.8	1.2				
2.8	1.0	4.5	$\infty$						
2.8	0.5	4.05	1.4	3.8	1.8	4.7	$\infty$		
2.8	0.35			3.85	2.4				
1.6	0.7			4.0	1.6	4.1	2.0		
Friction off, no close-in visual reference									
1.0	1.0			3.5–4.0	1.6–1.8				
Friction on									
0.5	0.15			4.1	1.1				
1.0	0.1			3.5	0.1				
1.0	0.2	3.5	0.8						

<sup>a</sup> $\infty$  means that no instability was found.

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1.6	0.7			4.0	1.6	4.1	2.0		
Friction off, no close-in visual reference									
1.0	1.0			3.5–4.0	1.6–1.8				
Friction on									
0.5	0.15			4.1	1.1	<b>Much stiffer (ideally rigid):</b> • no LCO • different BDFT frequencies			
1.0	0.1			3.5	0.1				
1.0	0.2	3.5	0.8						

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2.8	0.35			3.85	2.4				
1.6	0.7			4.0	1.6	4.1	2.0		
Friction off, no close-in visual reference									
1.0	1.0			3.5–4.0	1.6–1.8				
Friction on									
0.5	0.15			4.1	1.1	<b>Nominal:</b> • LCOs • at about twice nominal $G_c$			
1.0	0.1			3.5	0.1				
1.0	0.2	3.5	0.8						

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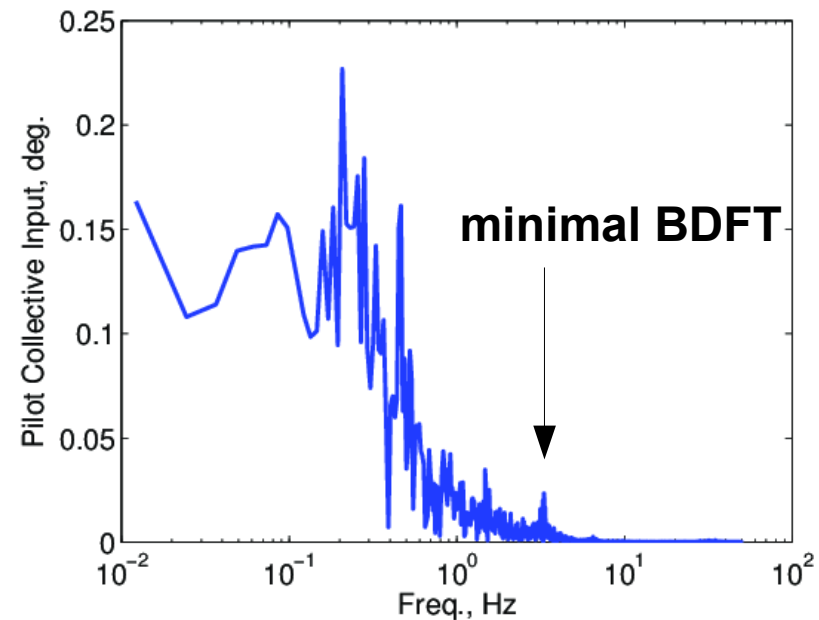
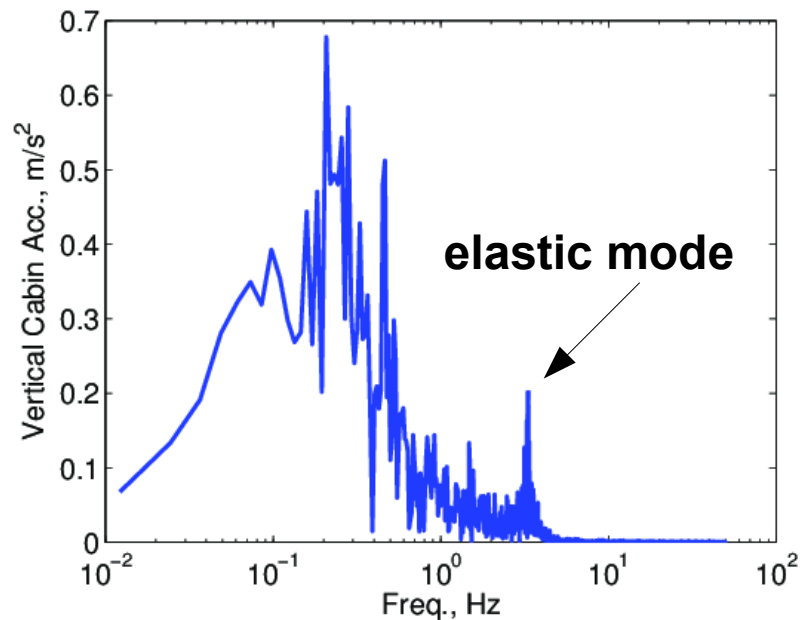
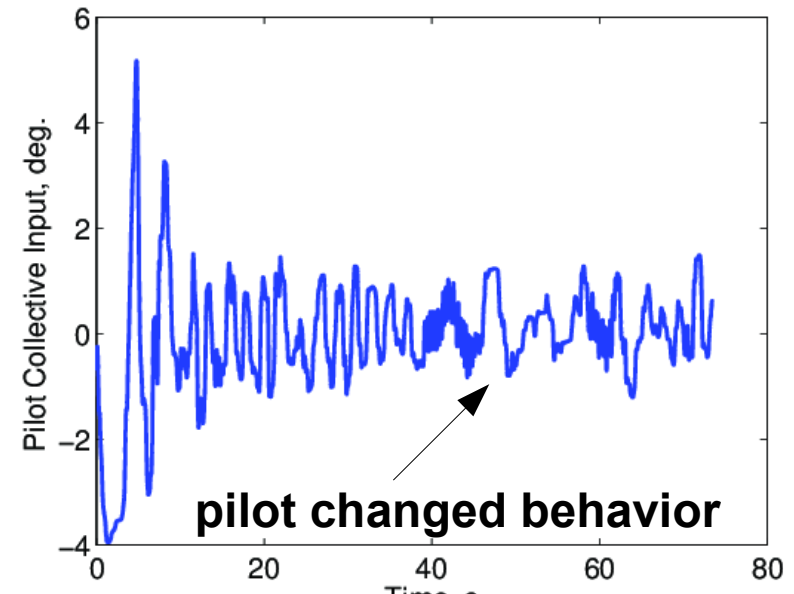
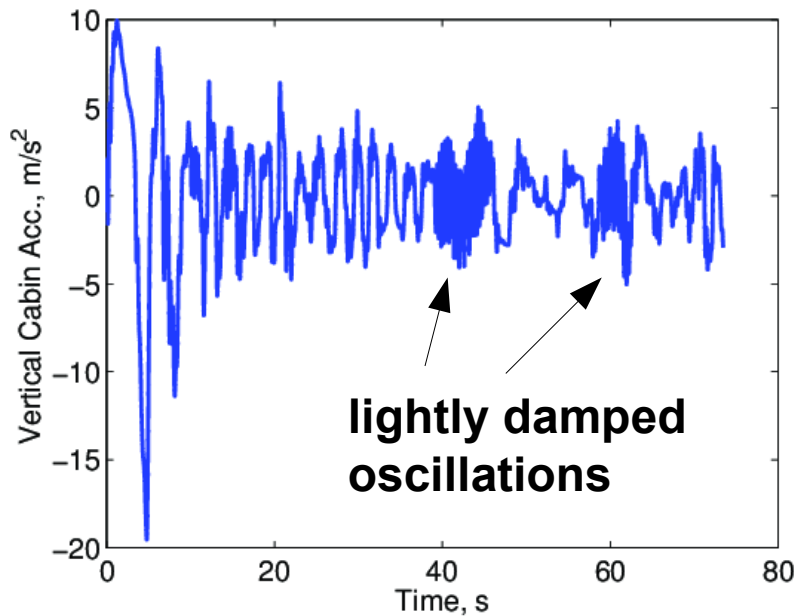
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1.6	0.4	3.98	0.4	3.8	1.2				
2.8	1.0	4.5	$\infty$						
2.8	0.5	4.05	1.4	3.8	1.8	4.7	$\infty$		
2.8	0.35			3.85	2.4				
1.6	0.7			4.0	1.6	4.1	2.0		
Friction off, no close-in visual reference									
1.0	1.0			3.5–4.0	1.6–1.8				
Friction on									
0.5	0.15			4.1	1.1	<b>Low stiffness &amp; damping:</b> • pronounced LCOs • quite variable $G_c$			
1.0	0.1			3.5	0.1				
1.0	0.2	3.5	0.8						



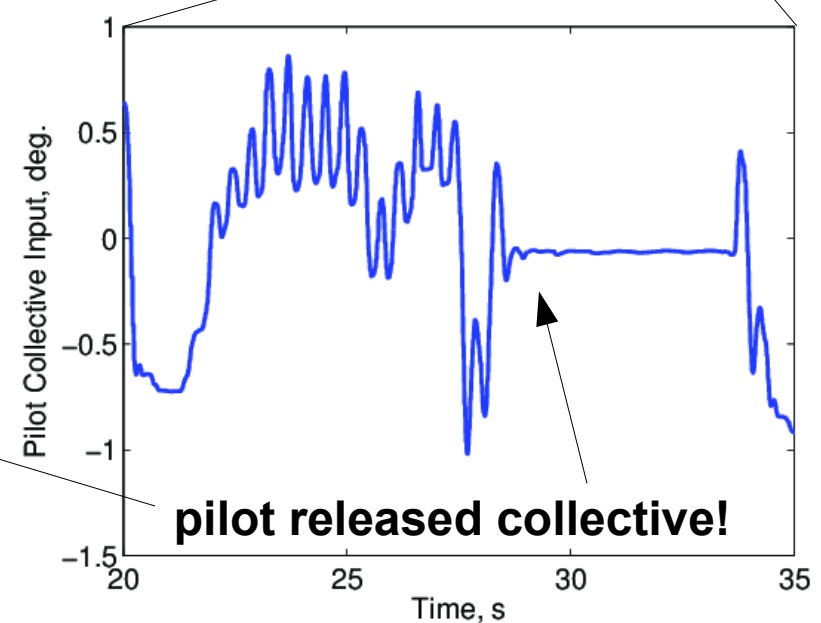
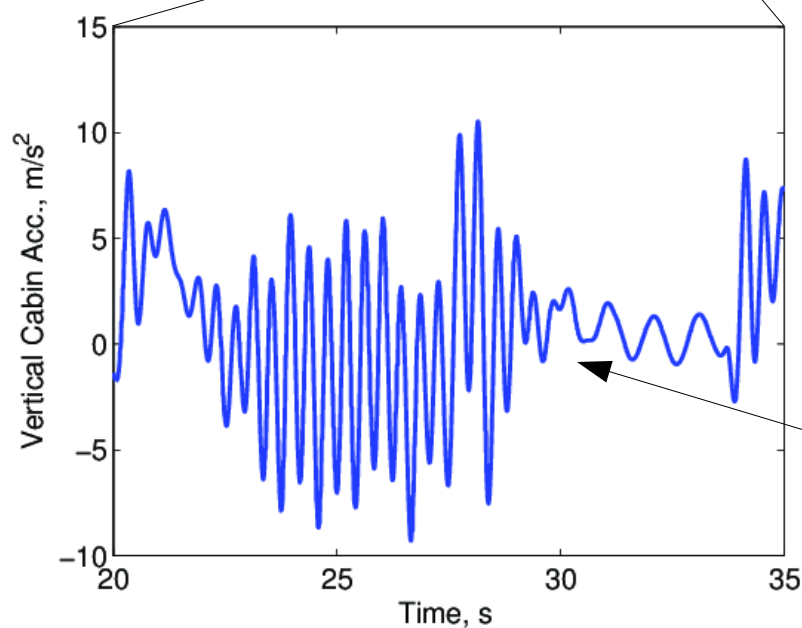
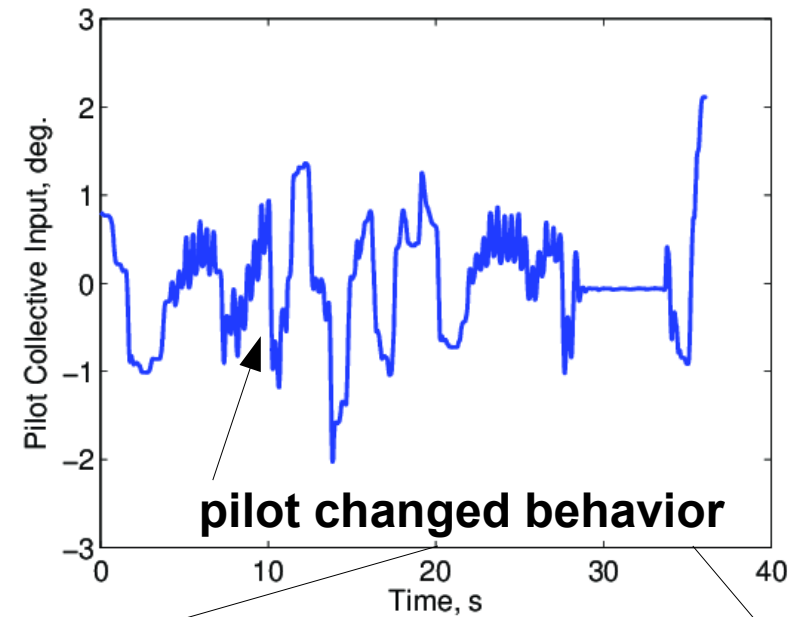
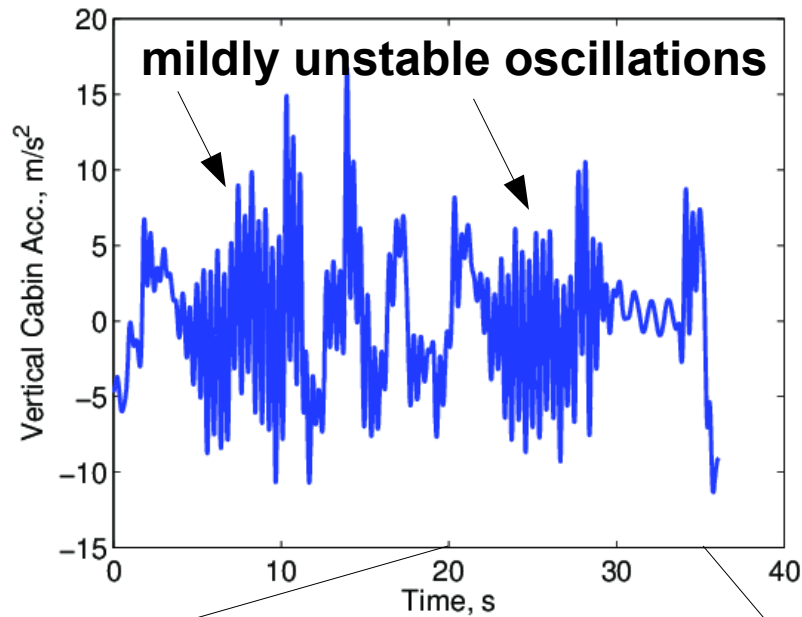
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## stable case

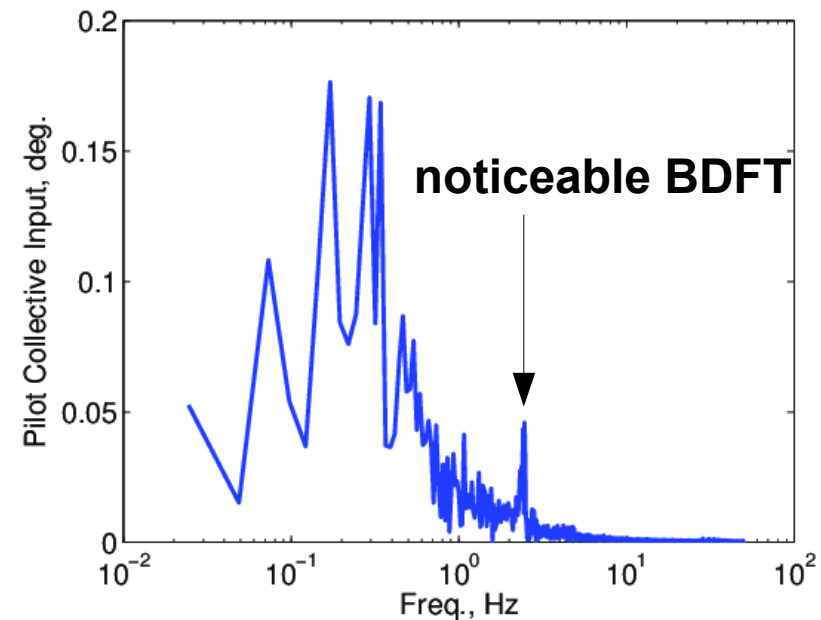
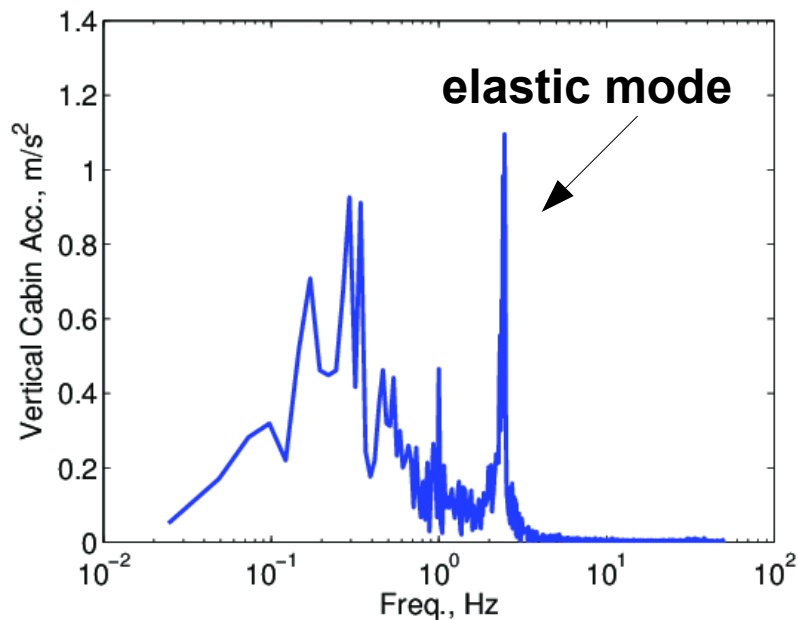
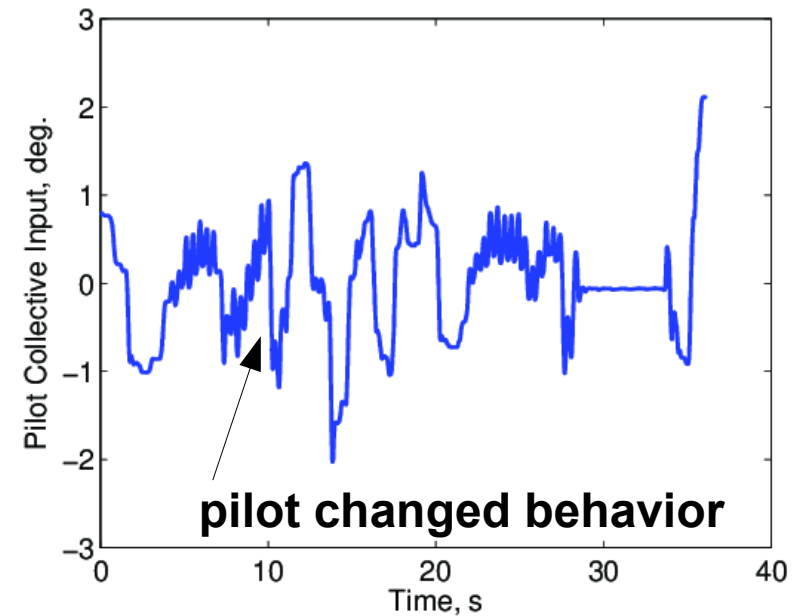
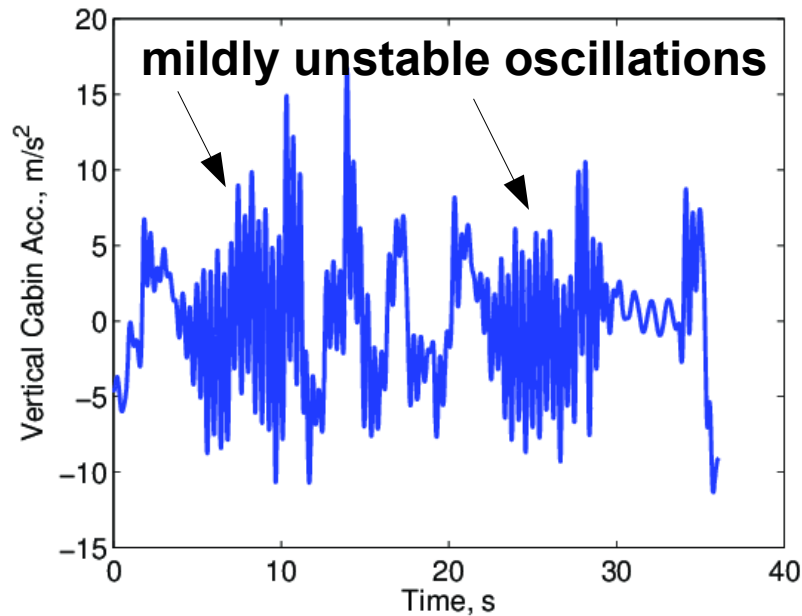




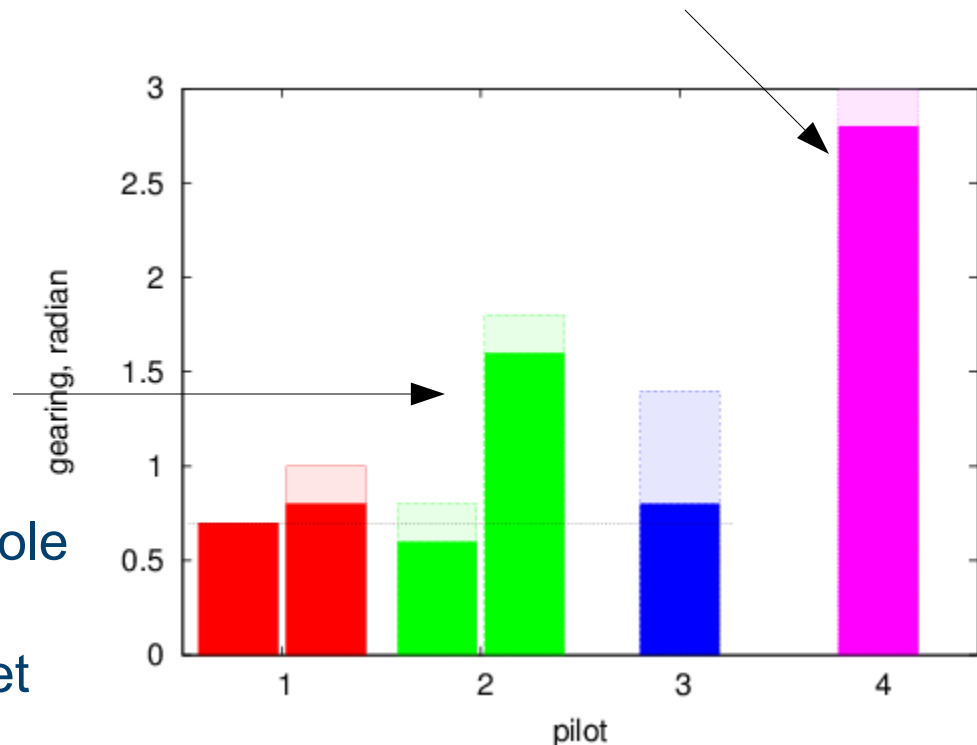
## marginally stable case



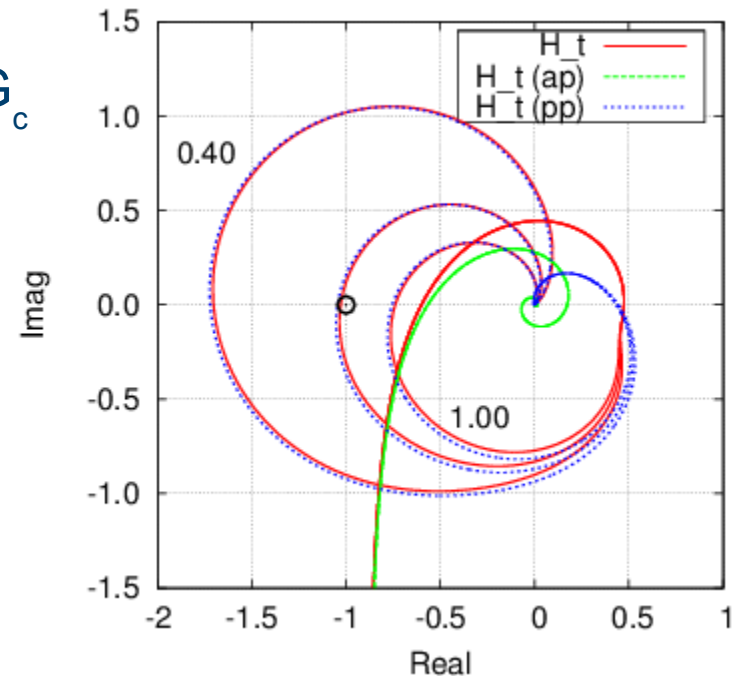
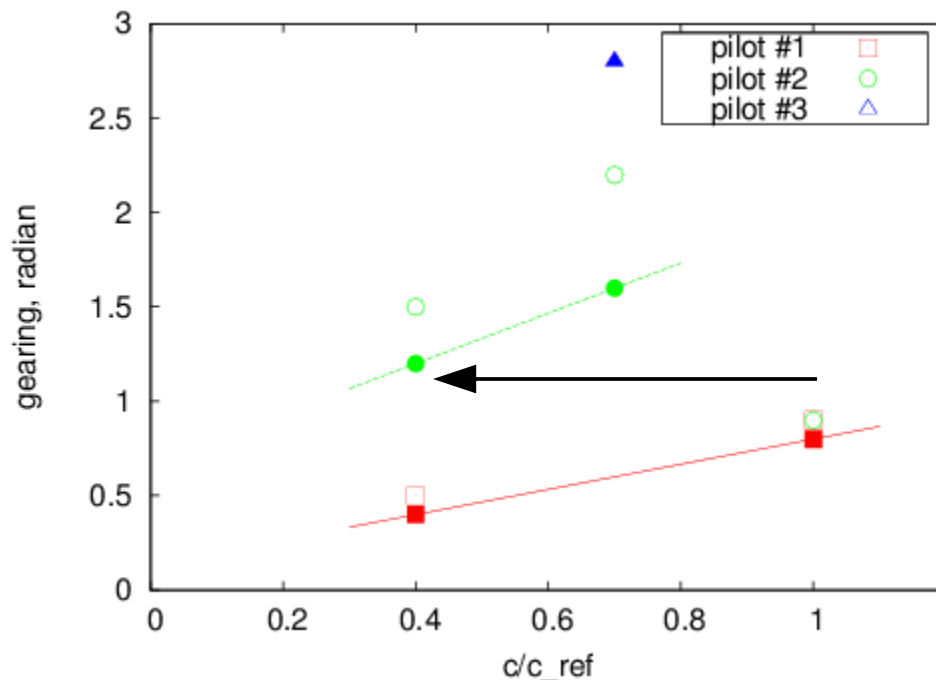
## marginally stable case



- Baseline case tested with all 4 occupants
- All non-professional pilots: LCO at about 3.5 Hz,  $G_c$  twice nominal
- Professional pilot (#4): LCO at about 2.8 Hz, blurred by intensive intentional activity (saturation? task dependent BDFT modification?)
- LCO at 2.8 Hz suggests biomechanic instability (elastic mode: 3.5 Hz)
- Pilot #2 shows instability at higher  $G_c$  when performing a similar task with different visual cueing environment (VCE): horizon instead of pole
- Pilot #1: LCO after alarm set by data acquisition system

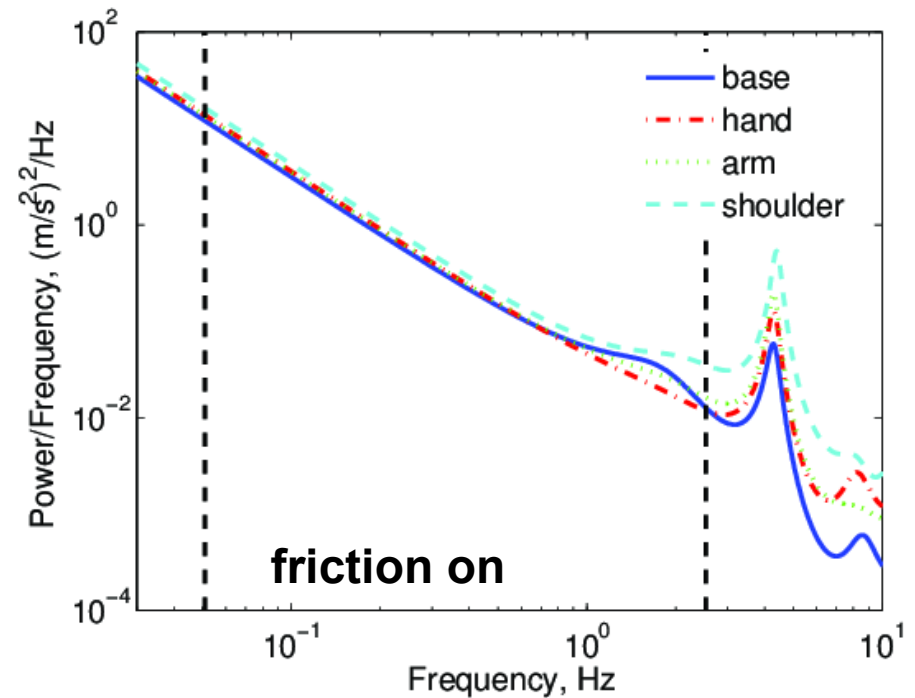
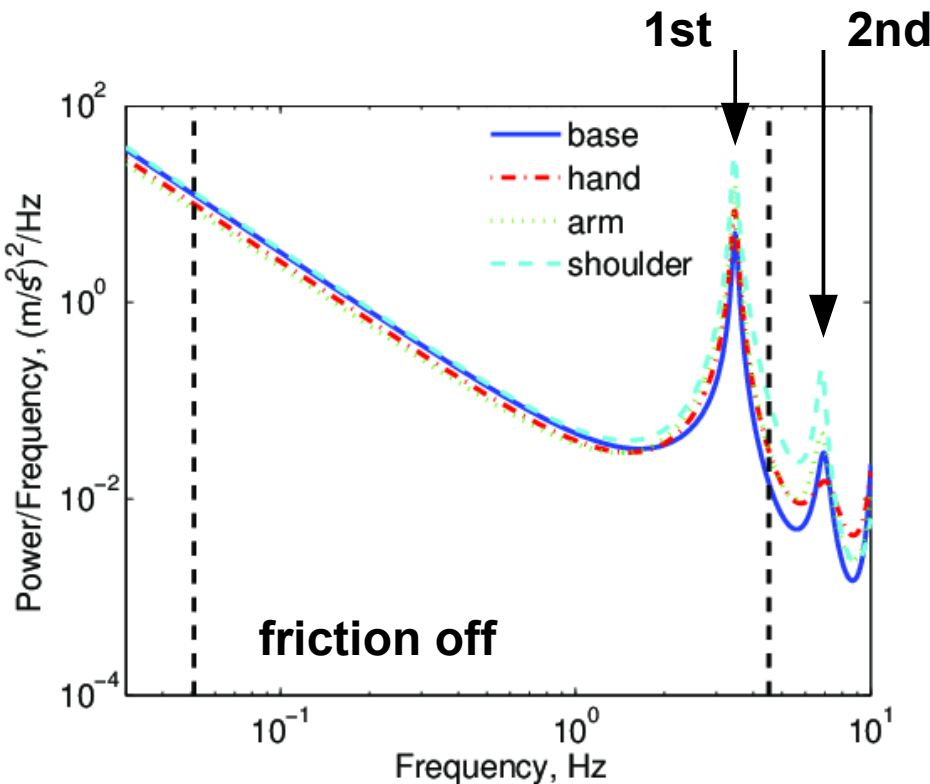


- Stiffer elastic mode:  $k/k_{\text{ref}} = 1.6$  and  $c/c_{\text{ref}} = 0.4, 0.7, 1.0$  (about 4.5 Hz)
- nominally unstable
- In practice, always stable w/ nominal  $G_c$ 
  - large variability amongst occupants
  - damping reduction result-driven



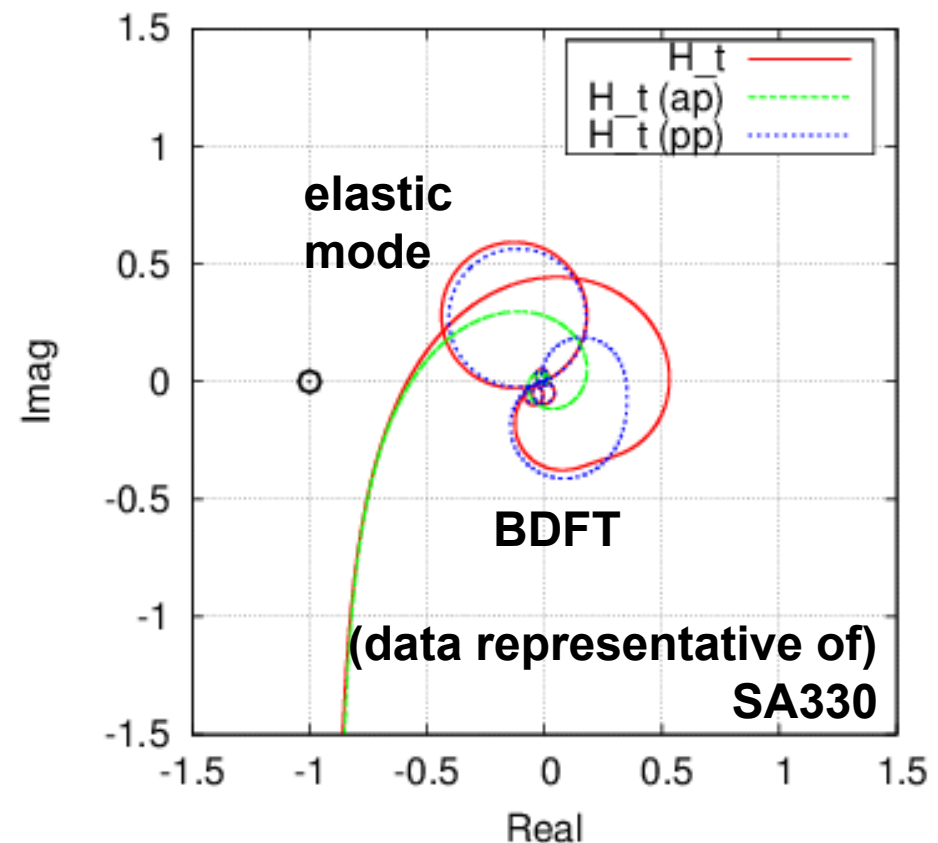
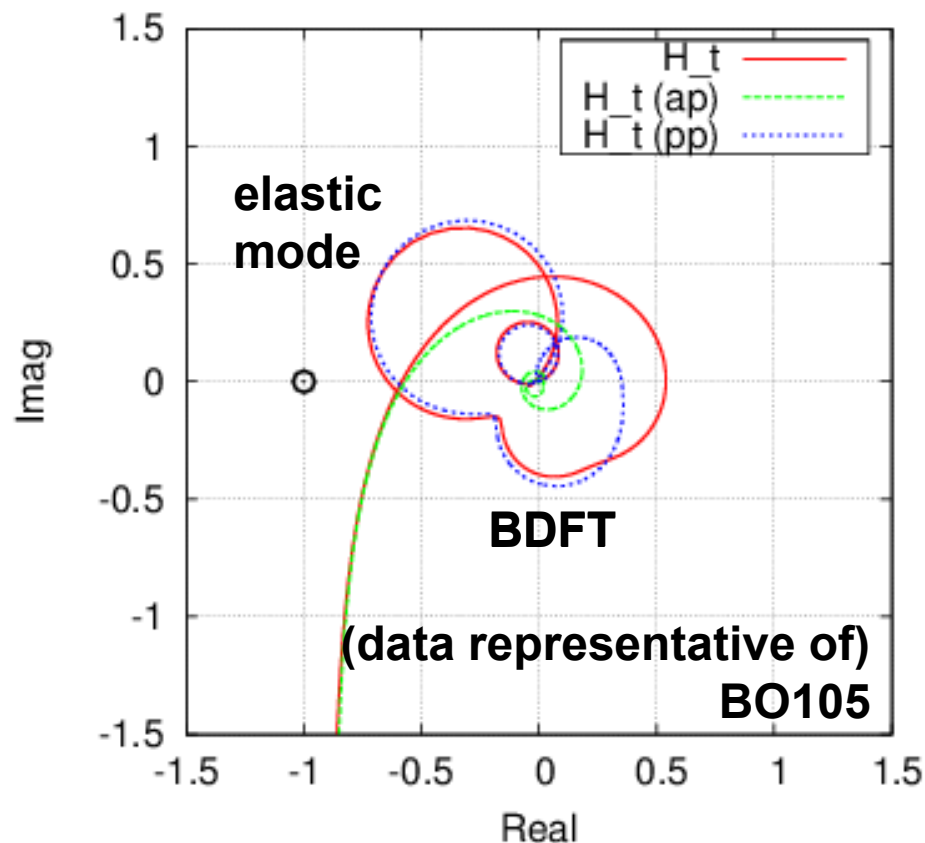
## Effect of friction:

- very low structural damping required for LCO to appear
- without friction, second harmonic of biomechanical mode appears
- with friction, only a biomechanical mode appears
- in a quasi-linear dynamics sense, friction represents equiv. damping



## Was this just a nice game? Analysis with deformable airframe model

- Clear similarities with simple aeroelastic model
- Typical light/medium helicopter relevant airframe dynamics show higher frequencies (6 to 9 Hz) than present (2.5 to 4.8 Hz)
- Interaction with pilot biomechanics less likely



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- Experimental investigation of helicopter pilot biomechanics
- Pilot-in-the-loop tests of simple marginally stable heave motion model
- Highlighted several aspects of helicopter-pilot interaction:
  - task dependence
  - variability among occupants, but clear common trends
  - instability caused by coupling of structural and biomech. modes
  - friction in control inceptor can alleviate but not eliminate the effect
  - results partially affected by saturation, especially at FM freq.
- Results partially scale on realistic airframe dynamics models



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**Thank you for your attention**

**Questions?**

MARIA

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