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Estimation in Aerospace

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School of Industrial and Information Engineering Aeronautical Engineering

- General information on the course.
- Overview of the course programme.



General information

- Marco Lovera
 - Dipartimento di Scienze e Tecnologie Aerospaziali
 - Tel. 02-23993592
 - email marco.lovera@polimi.it
- Meeting hours: Tuesday 14.30-16.30
- Course web page: accessible from

<http://www.aero.polimi.it/lovera>



- Schedule:

▪ Monday	14.30-16.15	BL27.12
▪ Tuesday	9.30-11.15	BL27.17
▪ Thursday	9.30-11.15	L0.2
▪ Thursday	16.30-18.15	BL27.15
- Composition of the course:
 - 50/55 lecture hours
 - 20/25 exercises and worked examplesfor a total of 8 CFU.



Exam

Two options available for the exam:

- oral exam
- a project.

There is no mid-semester test.



Prerequisites

- Main prerequisite: Fondamenti di Automatica or a similar course covering
 - System modeling: modelling concepts, state space models, examples.
 - Dynamic behavior: differential equations, qualitative analysis, stability.
 - Linear systems: matrix exponential, input/output response, linearisation.
 - Transfer functions: frequency domain modelling, transfer function, block diagrams, Bode plots, Laplace transform.
 - Frequency domain analysis: loop transfer function, Nyquist criterion, stability margins, generalised gain and phase.



Prerequisites

- Main prerequisite: basic background in probability and statistics
 - Random variable, probability, probability distribution and density functions.
 - Functions of random variables, mean, variance and moments.
 - Gaussian random variables.



- Teaching material
 - Slides are available for some (but not yet for all) topics
 - References to some specific textbooks and selected book chapters will be provided.



Motivation and objectives: parameter estimation and model identification

- The Fondamenti di Automatica course presents:
 - the basic methods and tools for mathematical modelling of dynamic systems
 - the fundamental concepts underlying the operation of feedback control systems
 - an introduction to the controller synthesis problem.
- The design of a control system however is a much more complex activity.
- In particular, the design approach studied in FdA is *model-based, i.e.*, it assumes that a model of the system exists.



Motivation and objectives: parameter estimation and model identification

Where can such a model come from?

Three typical situations that may occur:

- First principles modelling: basic laws of physics allow to derive a complete mathematical description of the system (white box modelling).
- First principle modelling with uncertain parameters: basic laws of physics allow to derive a complete model but some parameters are *uncertain*, e.g., damping ratios in a structure, aerodynamic coefficients *etc* (grey box modelling).
- No prior knowledge is available (black-box modelling).

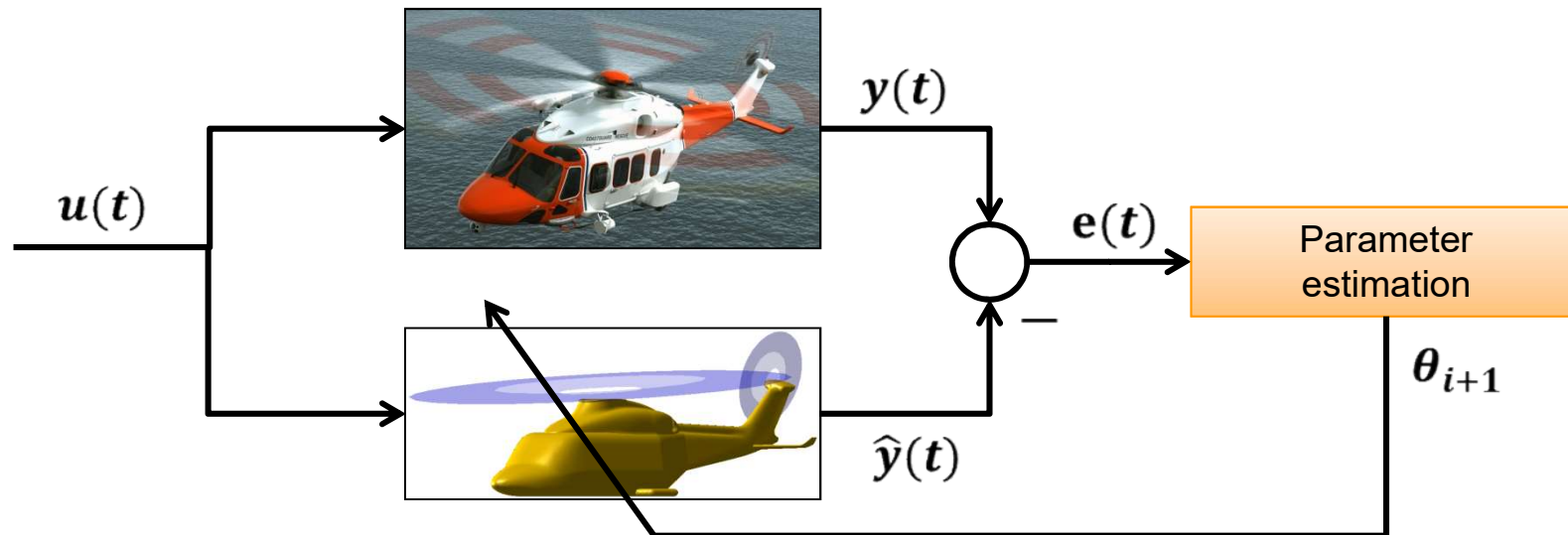
(many “shades of grey” can be defined between “grey” and “black”.)



Motivation and objectives: parameter estimation and model identification

In the second and third cases, DATA collected on the system can be used to obtain additional information and complete the model.

The question is: how does one find *optimal* models?





Example: sensor calibration

- A (stationary) accelerometer will measure Earth's gravitational field due to the reaction force on the mass within the MEMS structure
- A magnetometer will measure the Earth's magnetic field compounded with local magnetic interference
- For a calibrated sensor, the measured magnitude will be constant for all orientations

$$m = \|Ku - b\| = \textit{constant}$$

m : magnitude of the sensor's respective field

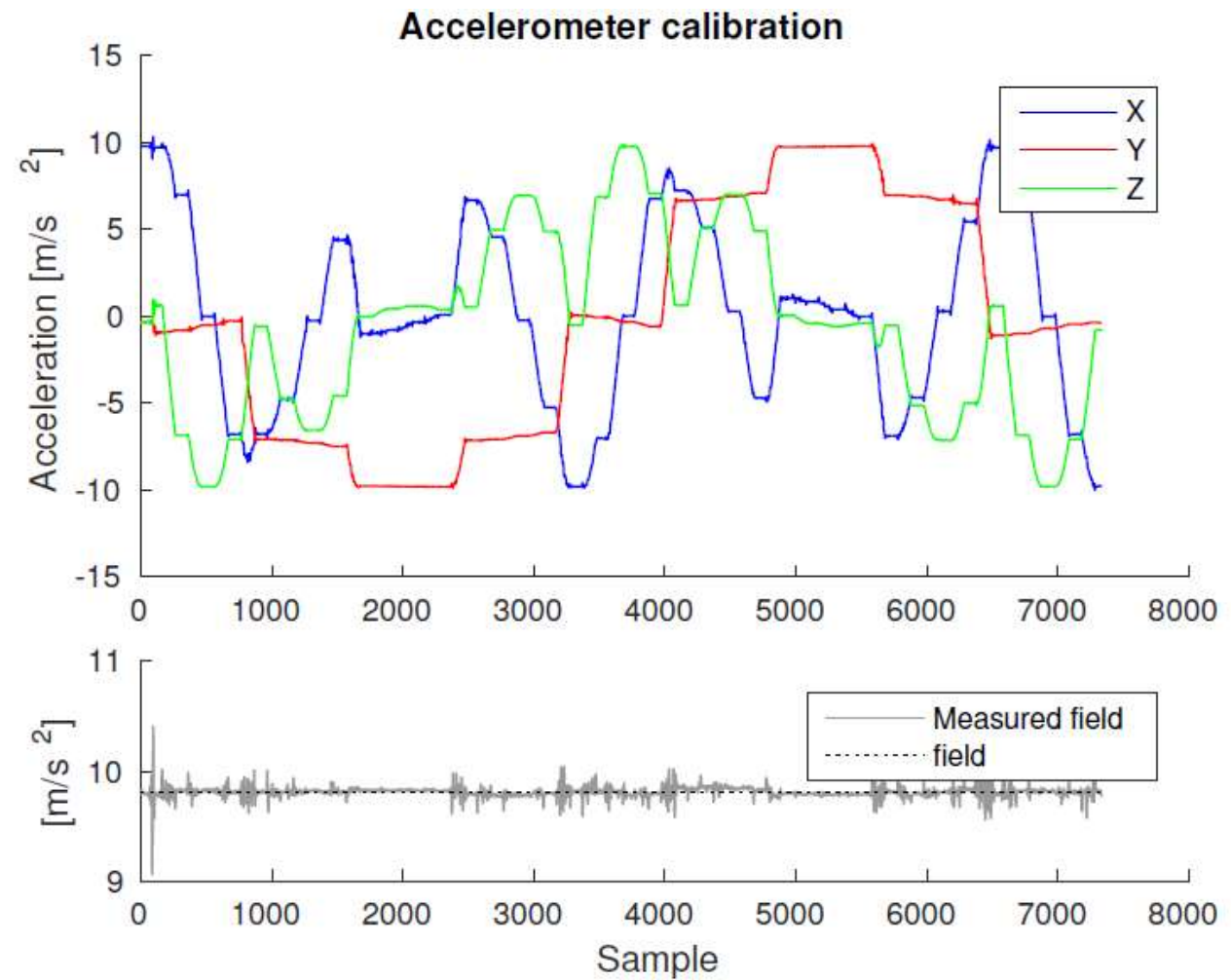
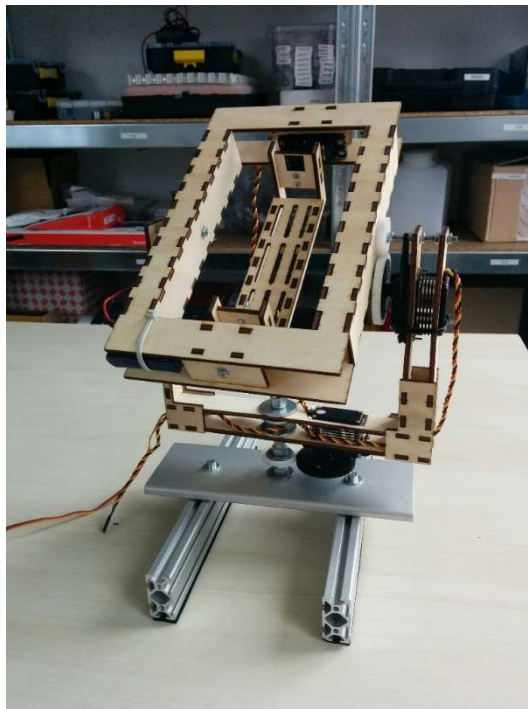
u : raw sensor measurement

K : matrix of calibration parameters

b : vector of biases



Example: sensor calibration

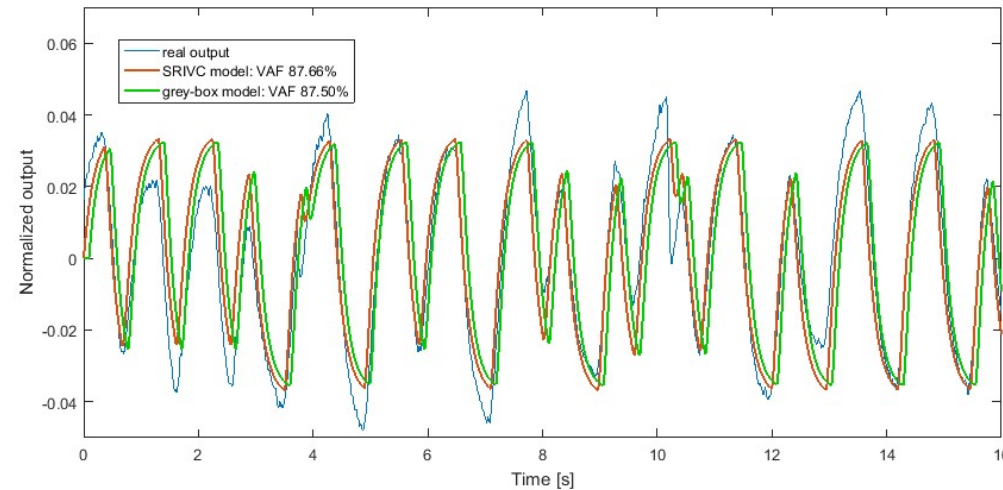
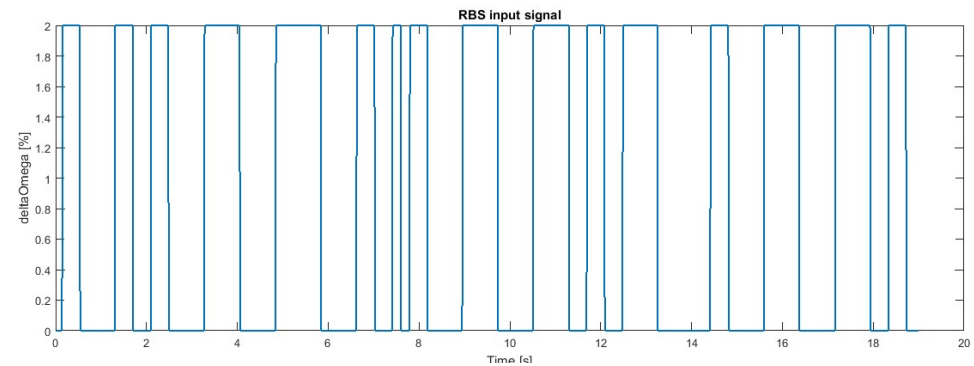




Example: single axis UAV attitude dynamics

- Simplified linearized roll dynamics:
$$\delta \dot{p} = \frac{1}{I_{xx}} \left[4K_t b \delta \Omega + \frac{\delta L}{\delta p} \delta p \right].$$
- Parameters to be identified:

Roll Inertia I_{xx} , Stability derivative $\frac{\delta L}{\delta p}$





Example: rotorcraft model identification

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- Consider the problem of characterizing helicopter dynamics near a given trim condition
- For helicopters the six-DOF state-space model must be considered, because of the strong inter-axis couplings
- Furthermore, body roll and rotor flapping are coupled as well
- This leads to a very complex model with many parameters





6-DOF dynamics



$$x = [u \quad v \quad w \quad p \quad q \quad r \quad \phi \quad \theta]$$

Forward flight at 80 knots



$$U_0 = 40 \frac{m}{s} \quad V_0 = 3 \frac{m}{s} \quad W_0 = -5 \frac{m}{s} \quad \Theta_0 = 0$$

State space model

$$\dot{u} = X_u u + X_v v + X_w w + X_p p + (X_q - W_0)q + (X_r + V_0)r - g\theta + X_{\delta_{lat}} \delta_{lat} + X_{\delta_{lon}} \delta_{lon} + X_{\delta_{ped}} \delta_{ped} + X_{\delta_{col}} \delta_{col}$$

$$\dot{v} = Y_u u + Y_v v + Y_w w + (Y_p + W_0)p + Y_q q + (Y_r - U_0)r + g\phi + Y_{\delta_{lat}} \delta_{lat} + Y_{\delta_{lon}} \delta_{lon} + Y_{\delta_{ped}} \delta_{ped} + Y_{\delta_{col}} \delta_{col}$$

$$\dot{w} = Z_u u + Z_v v + Z_w w + (Z_p - V_0)p + (Z_q + U_0)q + Z_r r + Z_{\delta_{lat}} \delta_{lat} + Z_{\delta_{lon}} \delta_{lon} + Z_{\delta_{ped}} \delta_{ped} + Z_{\delta_{col}} \delta_{col}$$

$$\dot{p} = L_u u + L_v v + L_w w + L_p p + L_q q + L_r r + L_{\delta_{lon}} \delta_{lon} + L_{\delta_{ped}} \delta_{ped} + L_{\delta_{col}} \delta_{col}$$

$$\dot{q} = M_u u + M_v v + M_w w + M_p p + M_q q + M_r r + M_{\delta_{lat}} \delta_{lat} + M_{\delta_{ped}} \delta_{ped} + M_{\delta_{col}} \delta_{col}$$

$$\dot{r} = N_u u + N_v v + N_w w + N_p p + N_q q + N_r r + N_{\delta_{lat}} \delta_{lat} + N_{\delta_{lon}} \delta_{lon} + N_{\delta_{ped}} \delta_{ped} + N_{\delta_{col}} \delta_{col}$$

$$\dot{\phi} = p$$

$$\dot{\theta} = q$$



Choice of outputs

$$y = [u \quad v \quad w \quad p \quad q \quad r \quad \phi \quad \theta]^T$$

State space model (with time delays)

$$M\dot{x}(t) = Fx(t) + Gu(t - \tau)$$

$$y(t) = H_1x(t) + H_2\dot{x}(t)$$

$$\tau = \begin{bmatrix} \tau_{lat} \\ \tau_{lon} \\ \tau_{ped} \\ \tau_{col} \end{bmatrix}$$



Motivation and objectives: parameter estimation and model identification

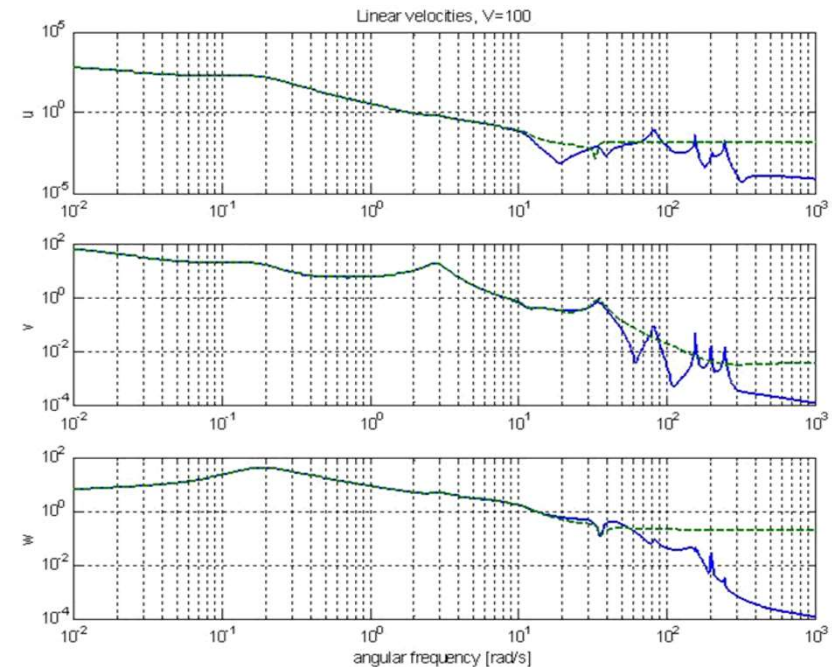
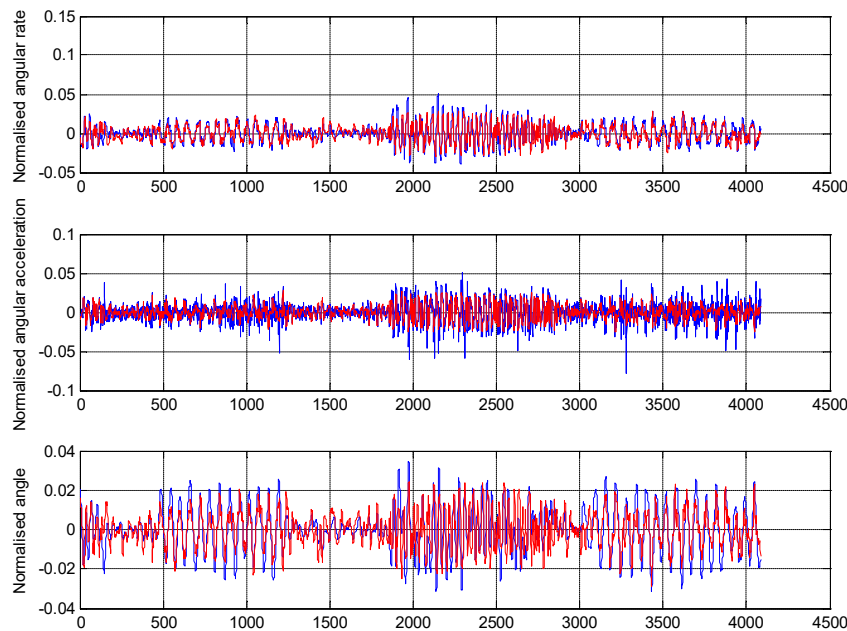
Typical questions to be faced:

- Grey box modelling: how do I derive a parametric model and how do I guarantee that the values of the parameters can be determined from data?
- Black-box modelling: how do I define the structure of the model and find the values of its parameters from data?



Motivation and objectives: parameter estimation and model identification

In the linear case problems can be formulated either in the *time-domain* or in the *frequency-domain*:

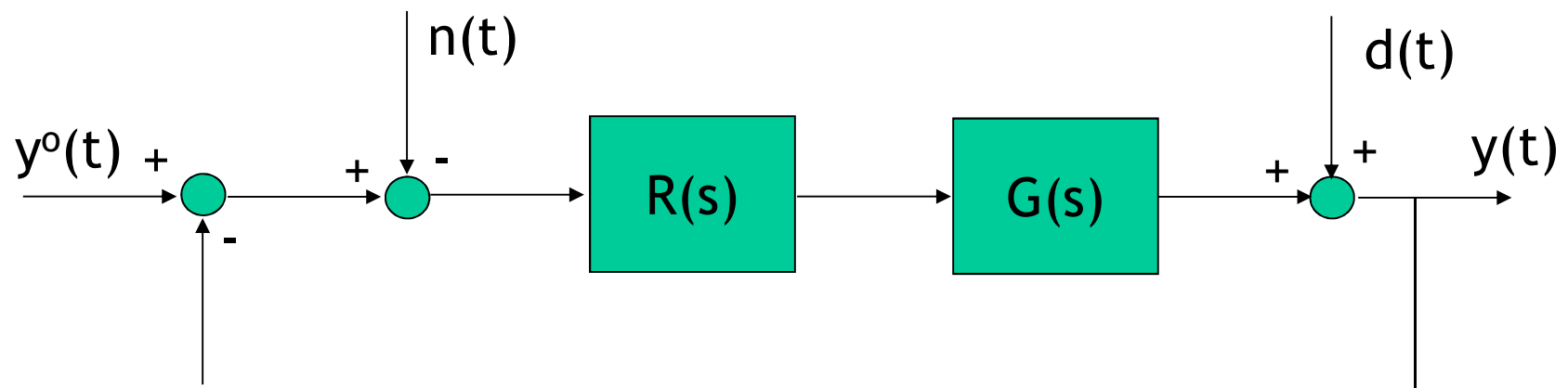


Both problems will be considered and extensions to nonlinear models will be studied (time-domain only).



Motivation and objectives: state estimation

In the elementary formulation of control design problems, it is assumed that the measured variable coincides with the controlled variable:





Motivation and objectives: state estimation

This however is not always true in practice.
Actually, it is hardly ever true in aerospace applications.

Typical situation:

design of flight control laws which aim at regulating

- attitude
- position

of an aircraft/rotorcraft/spacecraft using measurements of

- acceleration
- angular rate
- other variables such as magnetic field *etc.*



Motivation and objectives: state estimation

By referring, for the sake of simplicity, to a linear model, we have

$$\begin{aligned}\dot{x} &= Ax + Bu \\ y_1 &= C_1x + D_1u \\ y_2 &= C_2x + D_2u\end{aligned}$$

where y_1 is the measured output and y_2 is the (unmeasured) output to be controlled.

The estimation problem is then to compute an estimate of y_2 using measurements of u and y_1 and the model relating the variables.

If $y_2=x$ this is known as *state estimation*.



Example: attitude estimation for UAVs

Typically available measurements are provided by

- a tri-axial gyroscope,
- a tri-axial accelerometer and
- a tri-axial magnetometer mounted on the platform.

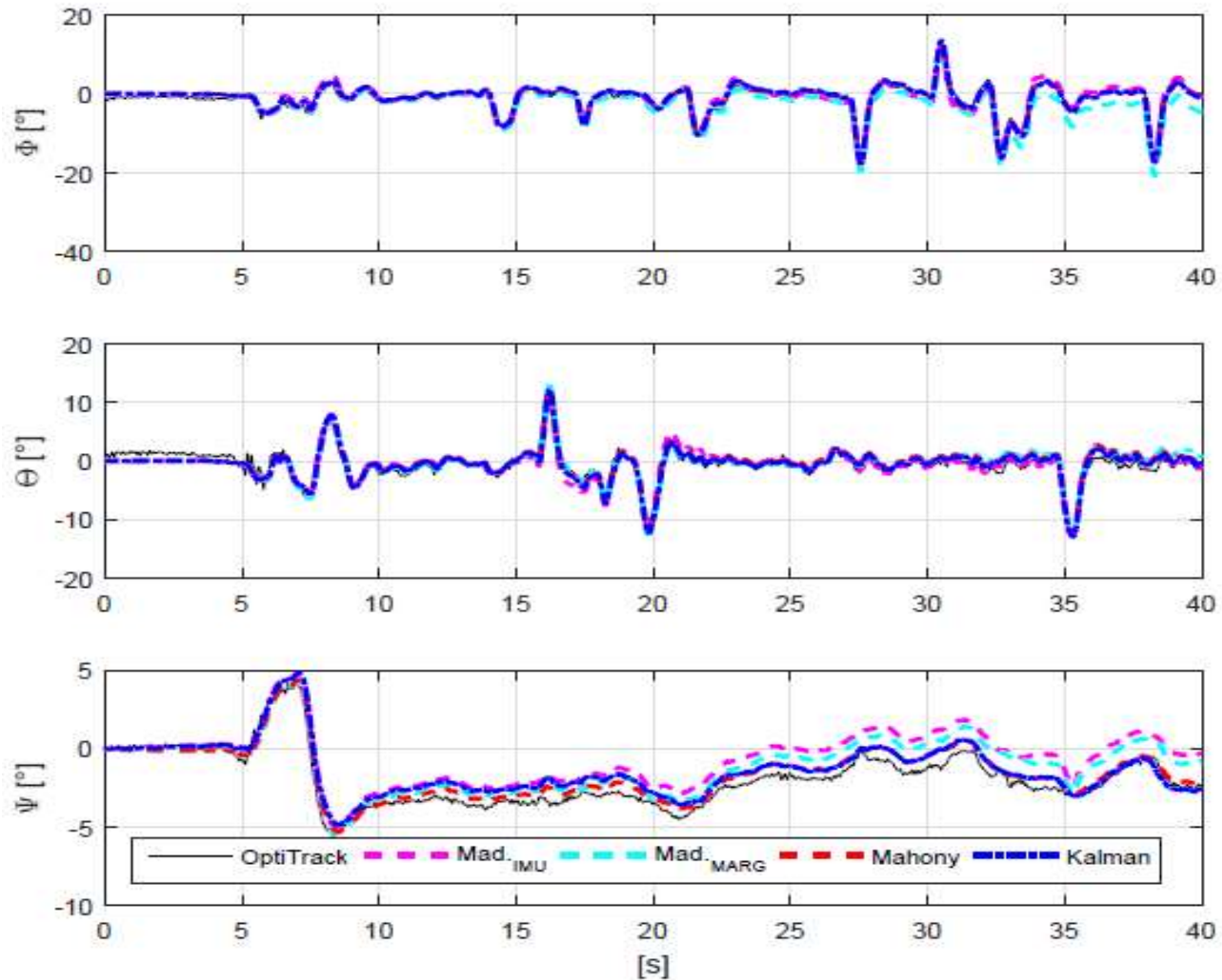
Problems to be faced:

- Write a model for the kinematics of the UAV
- Write a measurement model for each sensor
- Work out an algorithm – to be run on-board – which estimates the state variables in real time given the measurements.



Example: attitude estimation for UAVs

Sample results using different state estimation methods





Motivation and objectives: fault detection

Another critical problem in aerospace engineering is the detection of faults in, *e.g.*, control systems sensors.

The most common approach is *physical redundancy, i.e.*, using two or more functionally equivalent devices the outputs of which can be compared to improve reliability.

Alternative approach: *analytical redundancy, i.e.*, measured outputs are compared to model-based estimates and discrepancies are used to detect faults (or changes) in the system.



An example

Consider the linear, discrete-time system given by

$$x_k = \Phi x_{k-1} + w_{k-1}$$

$$z_k = Hx_k + v_k$$

$$\Phi = \begin{bmatrix} 0 & 1 \\ -0.4 & 0.6 \end{bmatrix}, \quad H = \begin{bmatrix} 1 & 0 \\ 1 & 0 \end{bmatrix},$$

$$Q = \sigma_w^2 I_2, \quad R = \sigma_v^2, \quad \sigma_w = 0.1, \quad \sigma_v = 0.01$$

Now we have two sensors measuring x_1 .

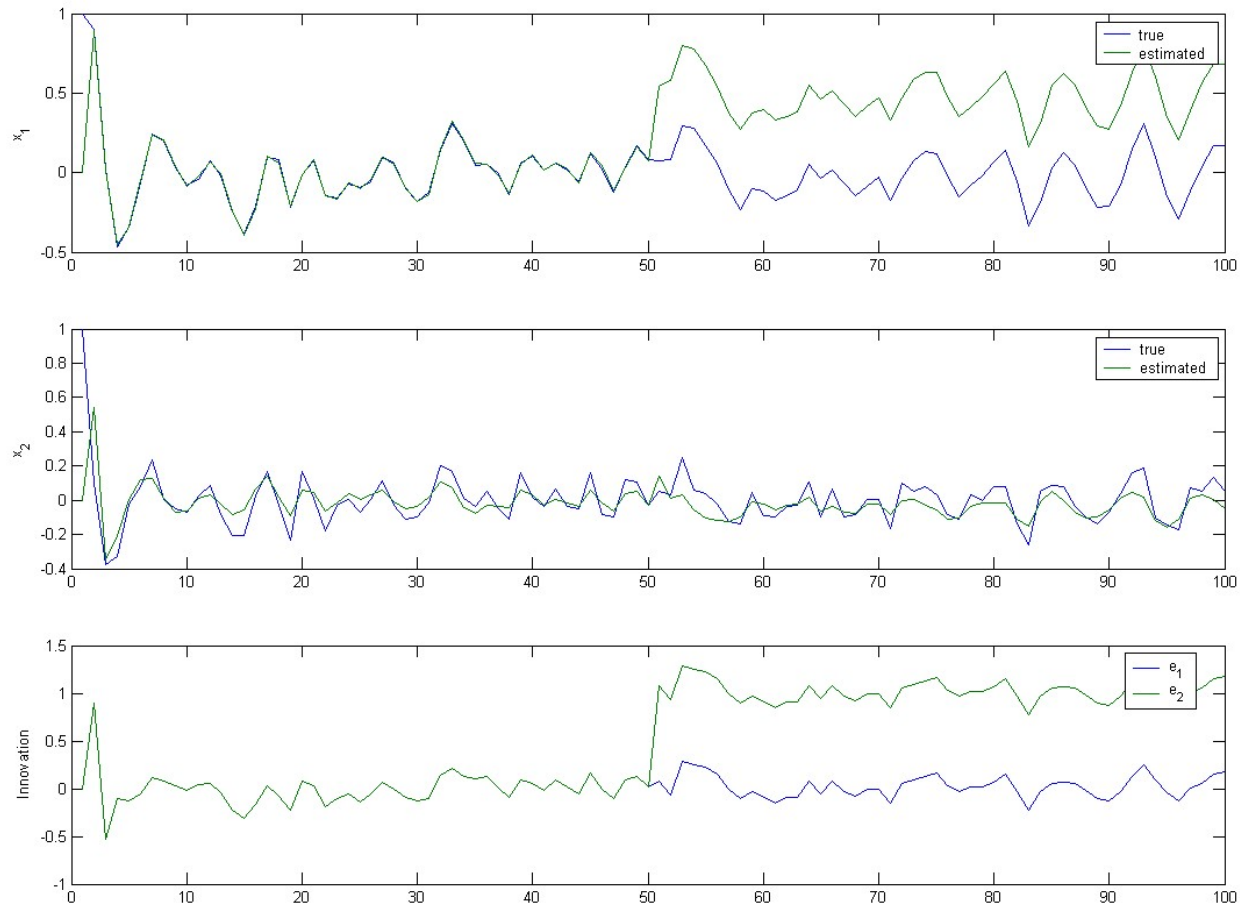
At time $k=50$, the second sensor becomes biased:

$$\{z_k\}_2 = \begin{bmatrix} 1 & 0 \end{bmatrix} x_k + v_k + 1, \quad k > 50$$



An example (2)

Simulation results





An example (3)

The problem with sensor 2 can be detected by monitoring $\{e_k\}_2$;

The faulty sensor can then be switched off;

If needed, a warning can be sent to a supervision system.



Motivation and objectives

In view of this, the Estimation in Aerospace course has the following objectives:

- to provide an introductory exposition to estimation theory, with specific reference to parameter estimation, state estimation and model identification.
- To study in greater depth some specific topics, namely:
 - Time-domain and frequency-domain parameter estimation for linear systems
 - State estimation for linear systems
 - Extensions to some classes of nonlinear systems.
- To illustrate the above by means of detailed case studies from aeronautics and space engineering.



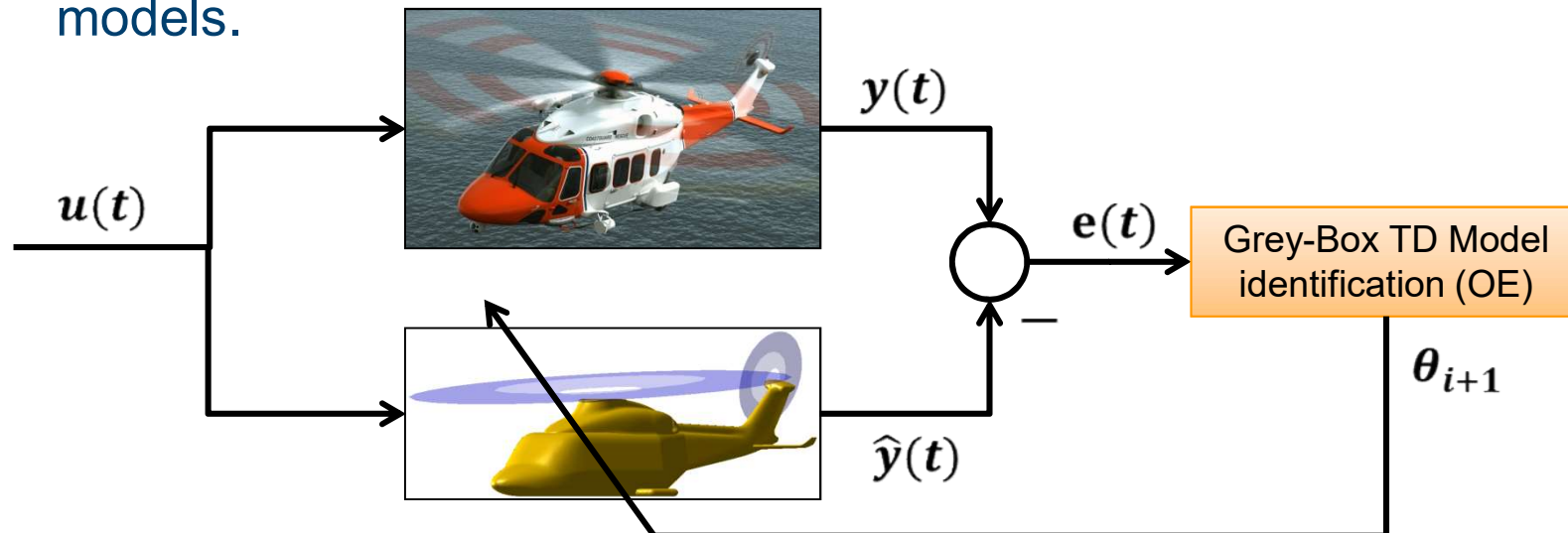
Part 1: introduction to estimation in aerospace.

- Overview of estimation problems in aerospace: sensor calibration, parameter estimation, model identification, state estimation, navigation, fault detection, fault tolerant control.
- Introduction to the theory of estimation
- Introduction to model identification: problem statement; grey vs black box models; linear vs nonlinear models; the notions of structural and experimental identifiability.
- The model identification process: from experiment design to model validation.



Part 2: parameter estimation and output error model identification

- Estimation theory: the maximum likelihood method; least squares estimation.
- Time-domain output error identification of linear state space models.
- Frequency-domain output error identification of linear state space models.
- Time-domain output error identification of nonlinear state space models.





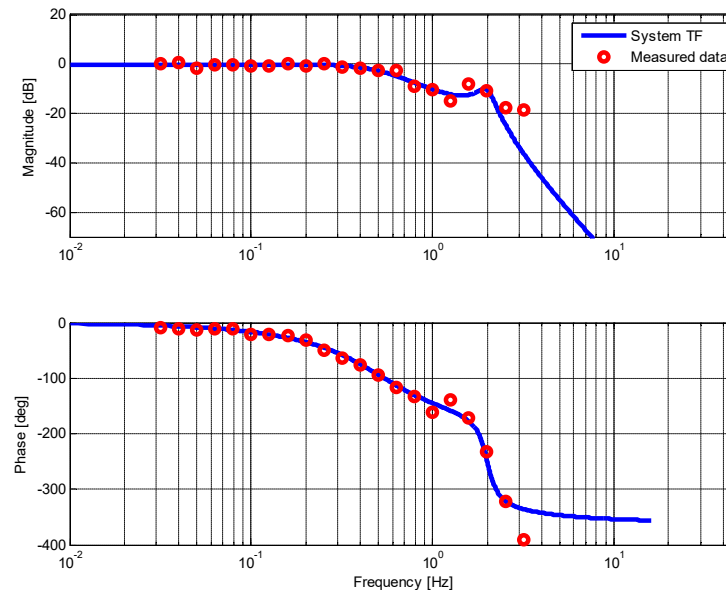
Part 3: state estimation and equation error model identification

- Estimation theory: introduction to Bayesian estimation.
- Optimal state estimation for linear systems: the Kalman filter.
- Time-domain equation error identification of linear state space models.
- State estimation for nonlinear systems: the Extended Kalman filter; overview of more general estimation schemes.
- Kalman filters: implementation issues.



Part 4: black-box linear model identification

- Problem statement: structure selection vs parameter estimation.
- Time- and frequency-domain identification of SISO linear models.
- Identification of MIMO linear models: introduction to subspace methods.





Part 5: case studies

- Identification of control-oriented models for helicopter flight mechanics.



- Attitude determination for a quadrotor UAV.
- Model-based control law design for small-scale and full-scale rotorcraft.