



 POLITECNICO DI MILANO



## Experiment design for MIMO model identification

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- Experiment design: fundamental role in the practice of model identification
- Problem of optimal experiment design has been studied extensively in the model identification literature
- The problem of defining optimal input sequences for MIMO model identification while taking into account operational constraints is considered
- Step-wise and multi-cyclic MIMO proposed methods are based on
  - C. Jauberthie, L. Denis-Vidal, P. Coton, and G. Joly-Blanchard. An optimal input design procedure. *Automatica*, 42(5):881-884, 2006.
  - D.E. Rivera, H. Lee, H.D. Mittelmann, and M.W. Braun. Constrained multisine input signals for plant-friendly identification of chemical process systems. *Journal of Process Control*, 19(4):623–635, 2009.



Excite the dynamic system so that the data contain sufficient information **respecting the constraints**

## **Constraints**

Inputs/outputs amplitude, experiment duration, system behaviour, etc.



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Inputs/outputs amplitude, experiment duration, system behaviour, etc.

## Non linear model

$$\dot{x} = f(x, u, \theta)$$

$$y = f(x, u, \theta)$$



*Equilibrium*  
 $\bar{x}, \bar{u} \Rightarrow \bar{y}$

$$x \in \mathbb{R}^n \quad u \in \mathbb{R}^q$$
$$y \in \mathbb{R}^m \quad \theta \in \mathbb{R}^p$$



Excite the dynamic system so that the data contain sufficient information **respecting the constraints**

## Constraints

Inputs/outputs amplitude, experiment duration, system behaviour, etc.

## Non linear model

$$\begin{aligned}\dot{x} &= f(x, u, \theta) \\ y &= g(x, u, \theta)\end{aligned}$$



*Equilibrium*  
 $\bar{x}, \bar{u} \Rightarrow \bar{y}$

$$\begin{aligned}x &\in \mathbb{R}^n & u &\in \mathbb{R}^q \\ y &\in \mathbb{R}^m & \theta &\in \mathbb{R}^p\end{aligned}$$

## Measured outputs

$$z(i) = y(iT_s) + v(i) \quad i = 1, 2, \dots, N$$

$$\begin{aligned}E[v(i)] &= 0 \\ E[v(i)v^T(j)] &= R\delta_{ij}\end{aligned}$$



### Fisher Information Matrix

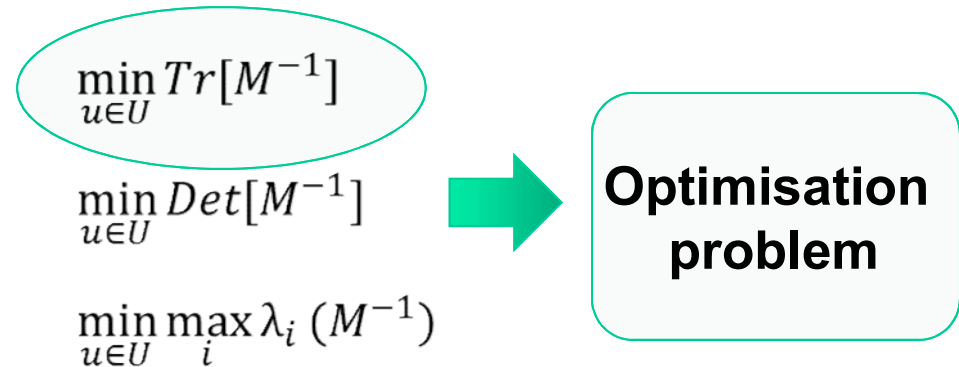
$$M = \sum_{i=1}^N \frac{\partial y(i)}{\partial \theta}^T R^{-1} \frac{\partial y(i)}{\partial \theta} \quad \text{Sensitivity } (x, \textcircled{u}, \theta)$$



Asymptotic variance of  $\theta_1$ :

$$M^{-1} = \begin{bmatrix} \sigma_1^2 & \dots & \dots \\ \vdots & \sigma_2^2 & \dots \\ \vdots & \vdots & \ddots \end{bmatrix}$$

Optimality criteria: scalar functions of  $M$



Linear SISO models



✓ Closed form solutions exist

Nonlinear MIMO models



✓ Numerical algorithms  
✓ *A priori* knowledge on  $\theta$



### Fisher Information Matrix

$$M = \sum_{i=1}^N \frac{\partial y(i)}{\partial \theta} R^{-1} \frac{\partial y(i)}{\partial \theta} \quad \text{Sensitivity } (x, \mathbb{u}, \theta)$$

### Optimisation Problem

$$\min_{u \in U} \text{Tr}[M^{-1}] = \sum_{i=1}^{n_p} \sigma_{\theta_i}^2$$

**Unconstrained problem is convex...**

**but the optimal solution might not be compatible with the dynamics!**





### Fisher Information Matrix

$$M = \sum_{i=1}^N \frac{\partial y(i)}{\partial \theta}^T R^{-1} \frac{\partial y(i)}{\partial \theta} \quad \text{Sensitivity } (x, \textcircled{u}, \theta)$$

### Constrained Optimisation Problem

$$\begin{aligned} \min_{u \in U} \text{Tr}[M^{-1}] \\ \text{s.t. } y \in Y \end{aligned}$$



### Fisher Information Matrix

$$M = \sum_{i=1}^N \frac{\partial y(i)}{\partial \theta} R^{-1} \frac{\partial y(i)}{\partial \theta} \quad \text{Sensitivity } (x, \textcircled{u}, \theta)$$

### Optimisation Problem

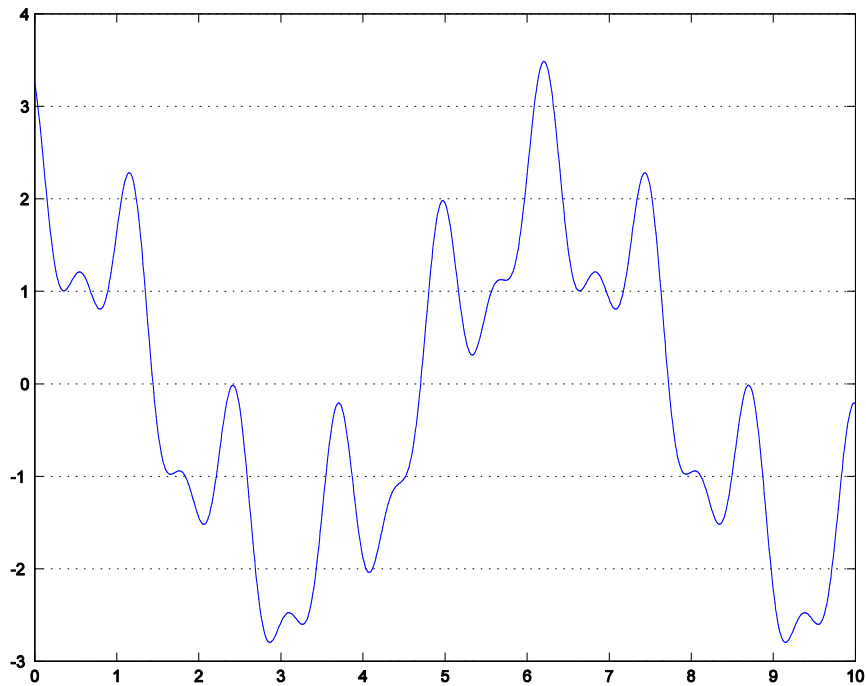
$$\begin{aligned} \min_{u \in U} \text{Tr}[M^{-1}] \\ \text{s.t. } y \in Y \end{aligned}$$

**Nonconvex problem** (except some cases)



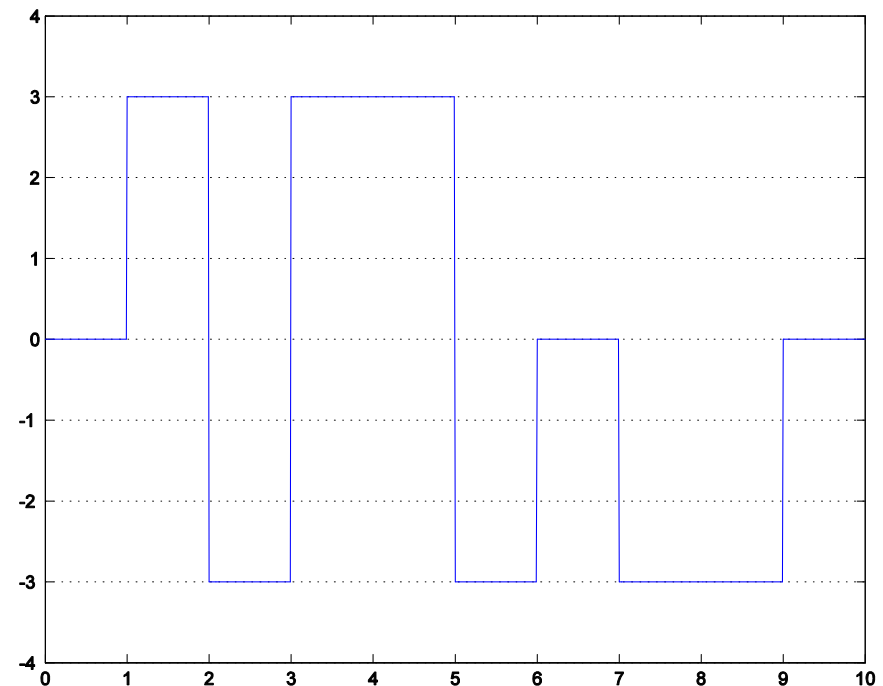
# Considered input signal classes

## Orthogonal multisines



✓ Automatic control system

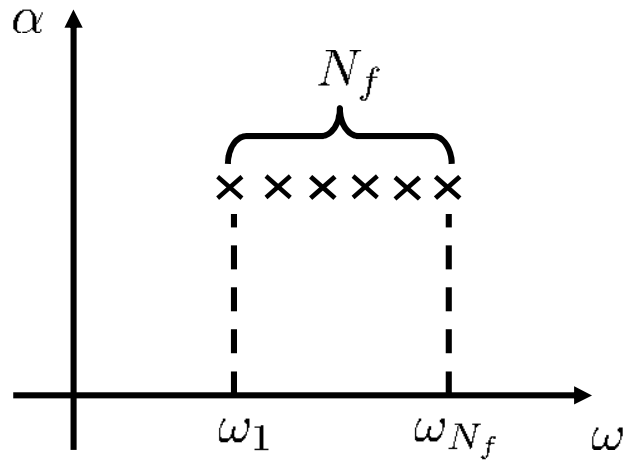
## Piecewise constant



✓ Pilot



## Single Input



$$u(t) = \bar{u} + \sum_{i=1}^{N_f} \alpha_i \cos(\omega_i t + \phi_i)$$

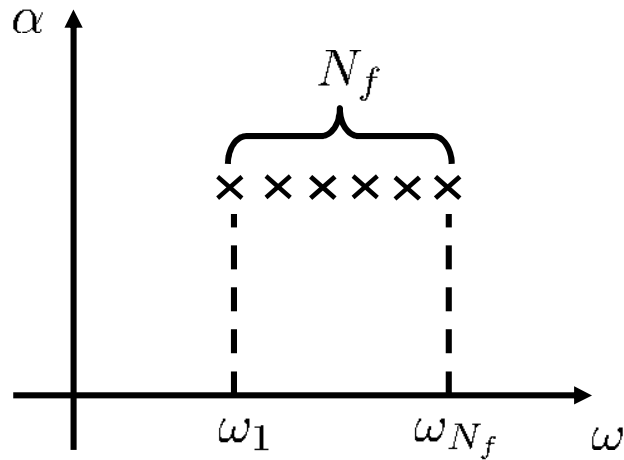
## Input design: parameters

- ✓ Bandwidth ( $\omega_1, \omega_{N_f}$ )
- ✓ Number of harmonics ( $N_f$ )
- ✓ Output constraints



# Multisine signals (SISO)

## Single Input



## Input design: parameters

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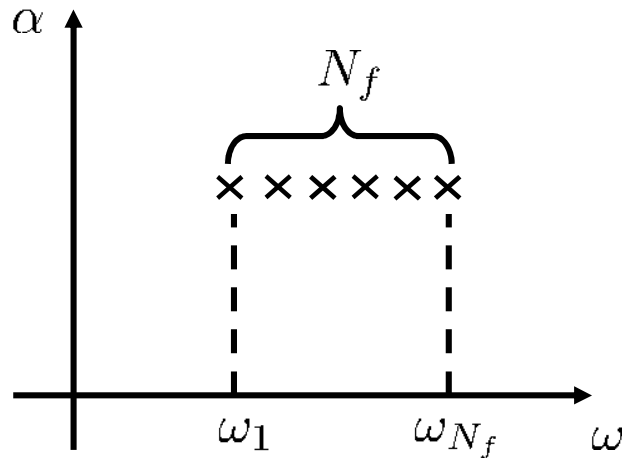
$$u(t) = \bar{u} + \sum_{i=1}^{N_f} \alpha_i \cos(\omega_i t + \phi_i)$$

Optimisation variables



# Multisine signals (SISO)

## Single Input



$$u(t) = \bar{u} + \sum_{i=1}^{N_f} \alpha_i \cos(\omega_i t + \phi_i)$$

Optimisation variables

### Initial solution

Amplitudes ( $\alpha_i$ )  $\Rightarrow$  Uniform  
Phases ( $\phi_i$ )  $\Rightarrow$  Schroeder

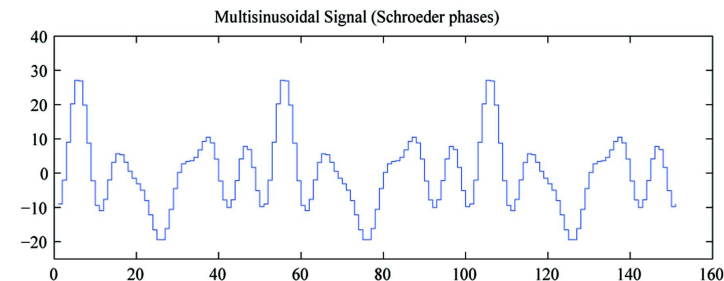
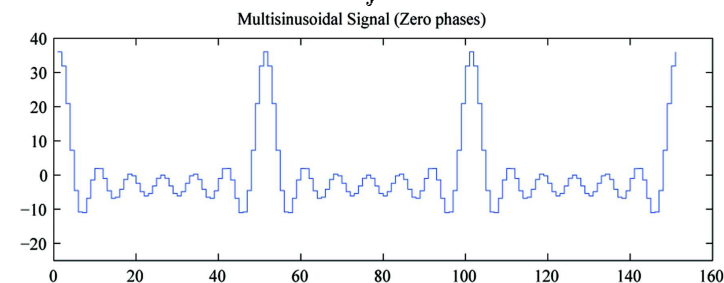
## Input design: parameters

- ✓ Bandwidth ( $\omega_1, \omega_{N_f}$ )
- ✓ Number of harmonics ( $N_f$ )
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## Schroeder's phases

$$\phi_1 = 0$$

$$\phi_i = \phi_{i-1} - \frac{\pi i^2}{N_f} \quad i = 2, 3 \dots N_f.$$

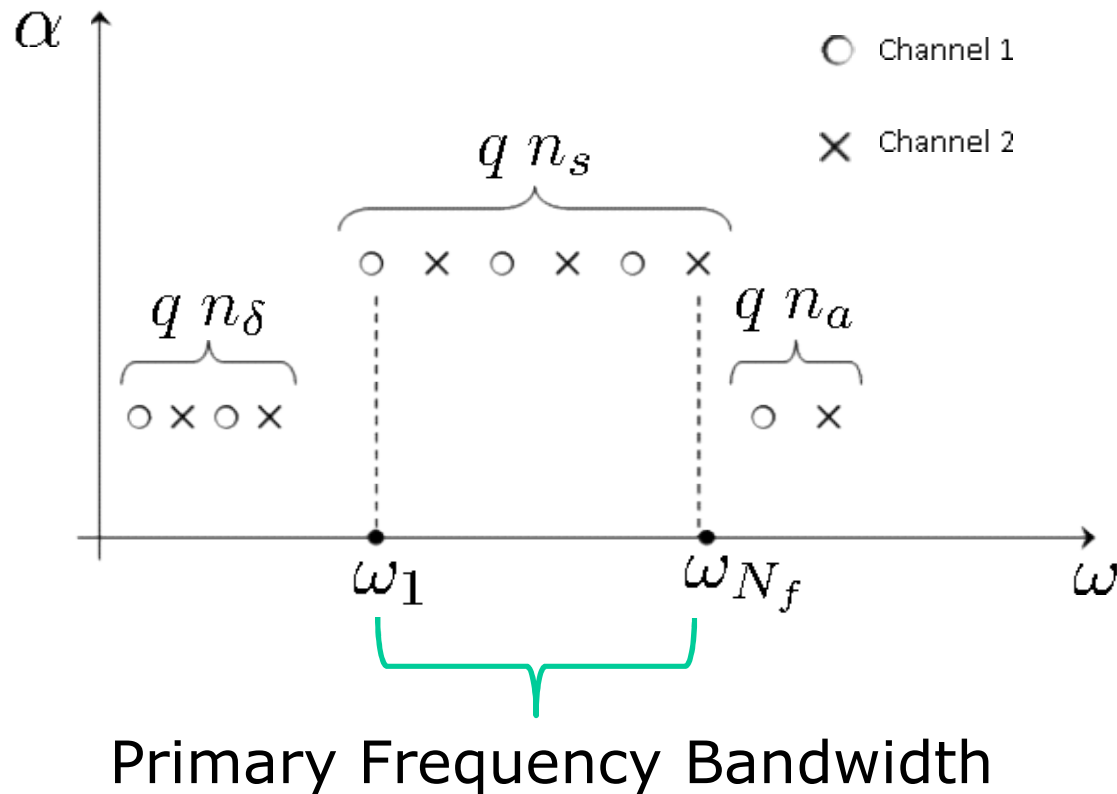




# Multisine signals (MIMO) - 1

## Multiple Input Design (Rivera et al. 2009)

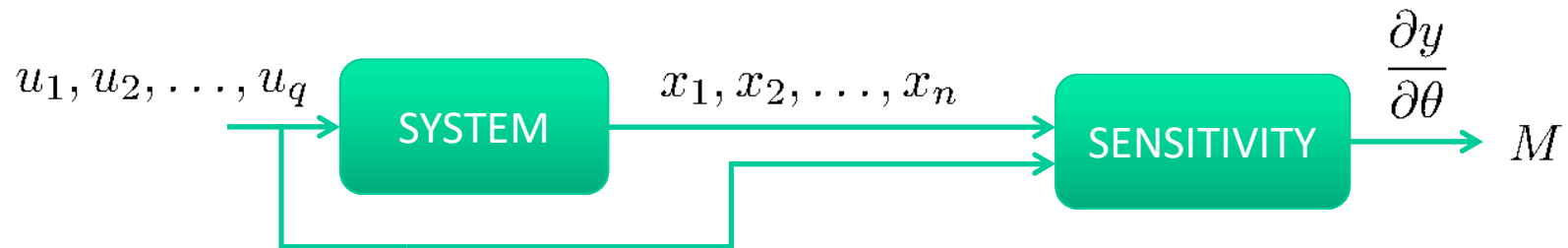
Different harmonic frequencies  Orthogonality between signals





## Multisine signals (MIMO) - 2

Optimisation problem  $\min_{u \in \mathcal{U}} \text{Tr}[M^{-1}]$



### Optimisation variables

- ✓ Harmonics amplitude ( $\alpha_{ij}$ )
- ✓ Harmonics phase ( $\phi_{ij}$ )

### Constraints

- ✓ Input amplitude  $u_i(t)$  s.t.  $|u_i(t) - \bar{u}| \leq \varepsilon_i \forall t, i = 1, \dots, q$
- ✓ Output amplitude  $y_i(t)$  s.t.  $|y_i(t) - \bar{y}| \leq \mu_i \forall t, i = 1, \dots, m$



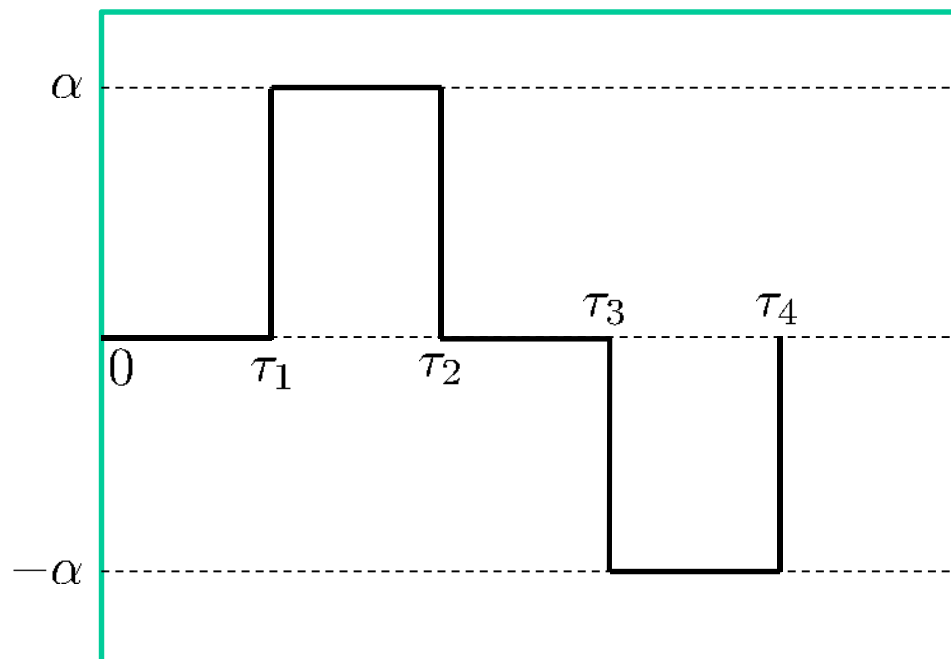


# Piecewise constant signals - 1

## First Step

$$u(t) = \bar{u} + \sum_{k=1}^r (\alpha \varepsilon_k - \alpha \varepsilon_{k-1}) H(t - \tau_k)$$

Input



(Jauberthie et al. 2006)

## Input Design Parameters

- ✓ Number of steps ( $r$ )
- ✓ Duration of each step ( $\tau_k$ )
- ✓ Maximum step amplitude ( $\alpha$ )
- ✓ Output constraints
- ✓ Experiment duration

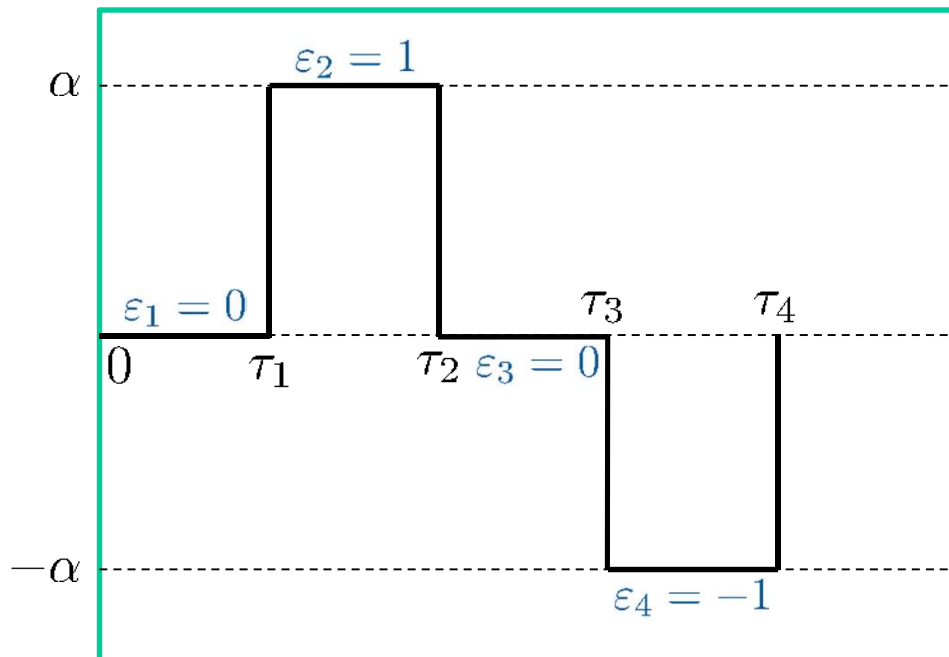


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## Optimisation

- ✓ Signal shape  $u(t) \longrightarrow (\varepsilon_k)$   
 $\varepsilon_k \in \{-1, 0, 1\}$

**Large number of solutions ( $3^r$ )**

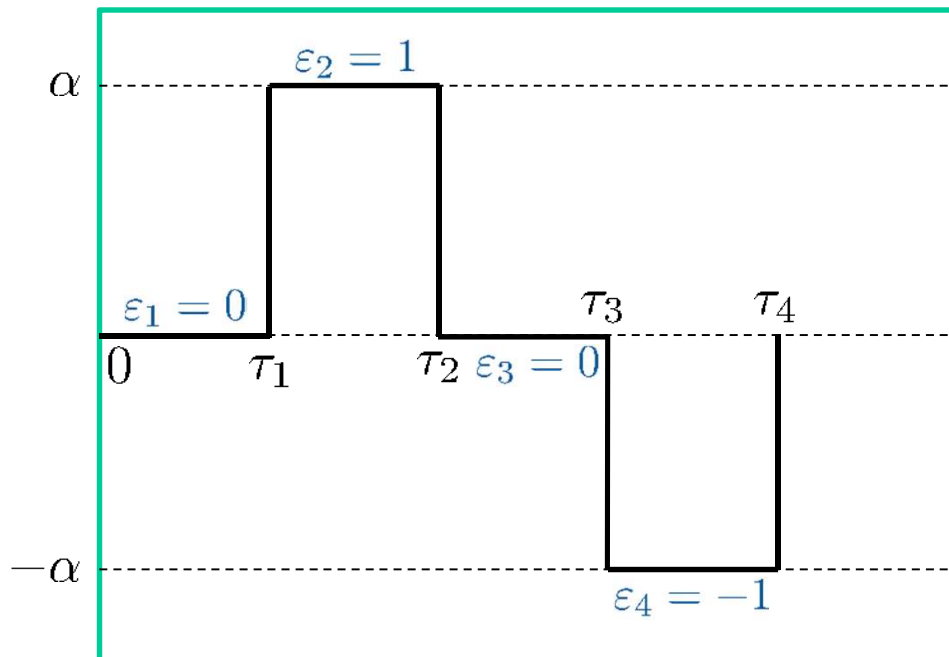


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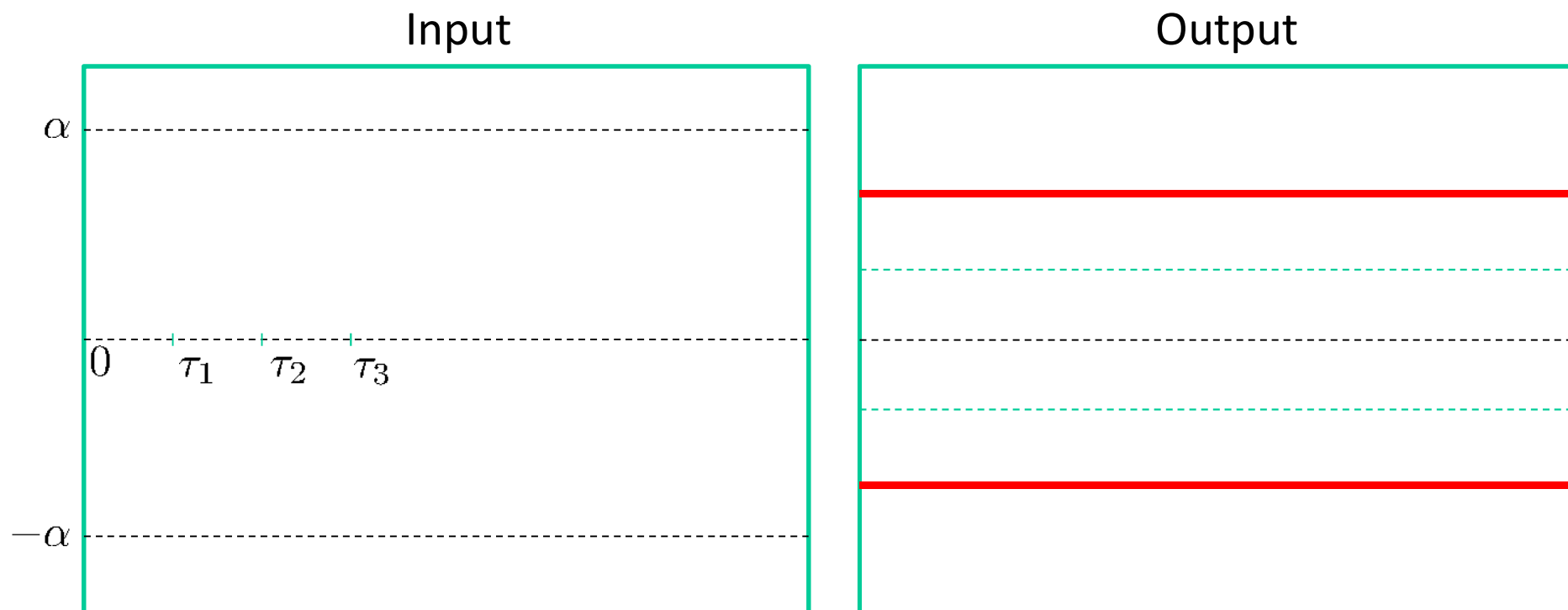
Dynamic programming



# Piecewise constant signals - 2

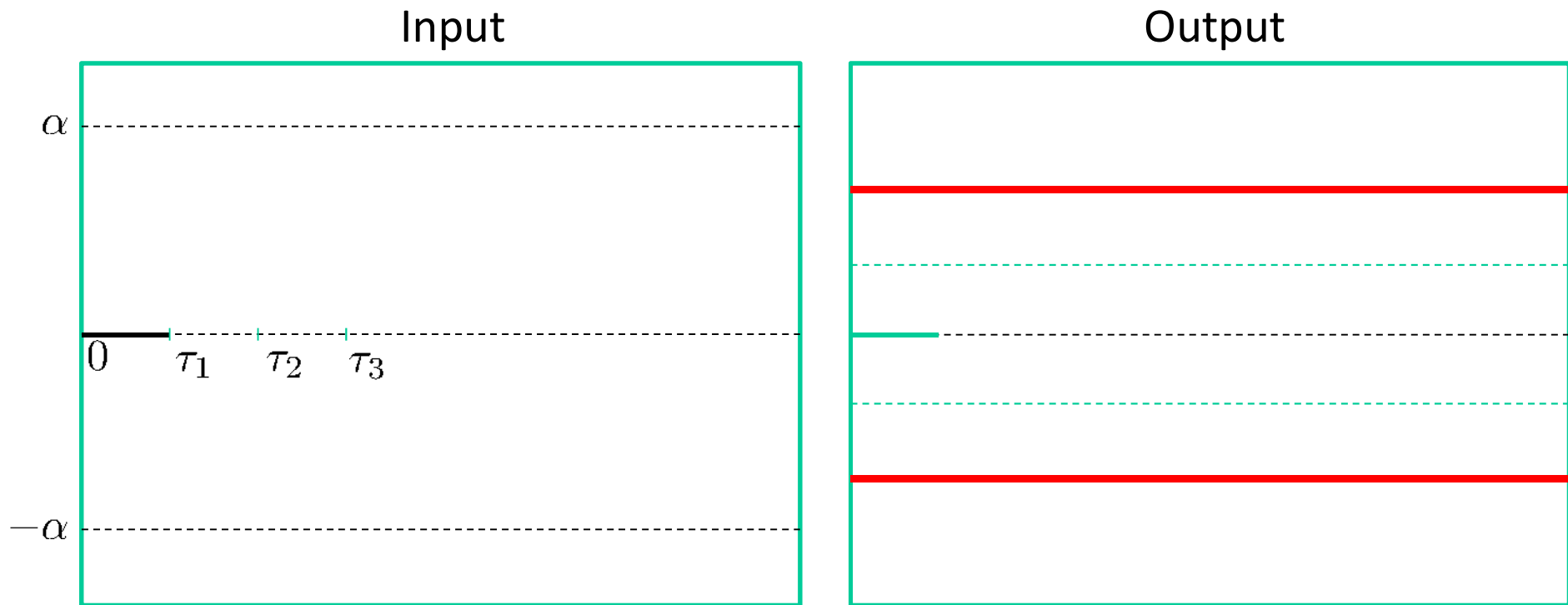


Example: **SISO** case



# Piecewise constant signals - 2

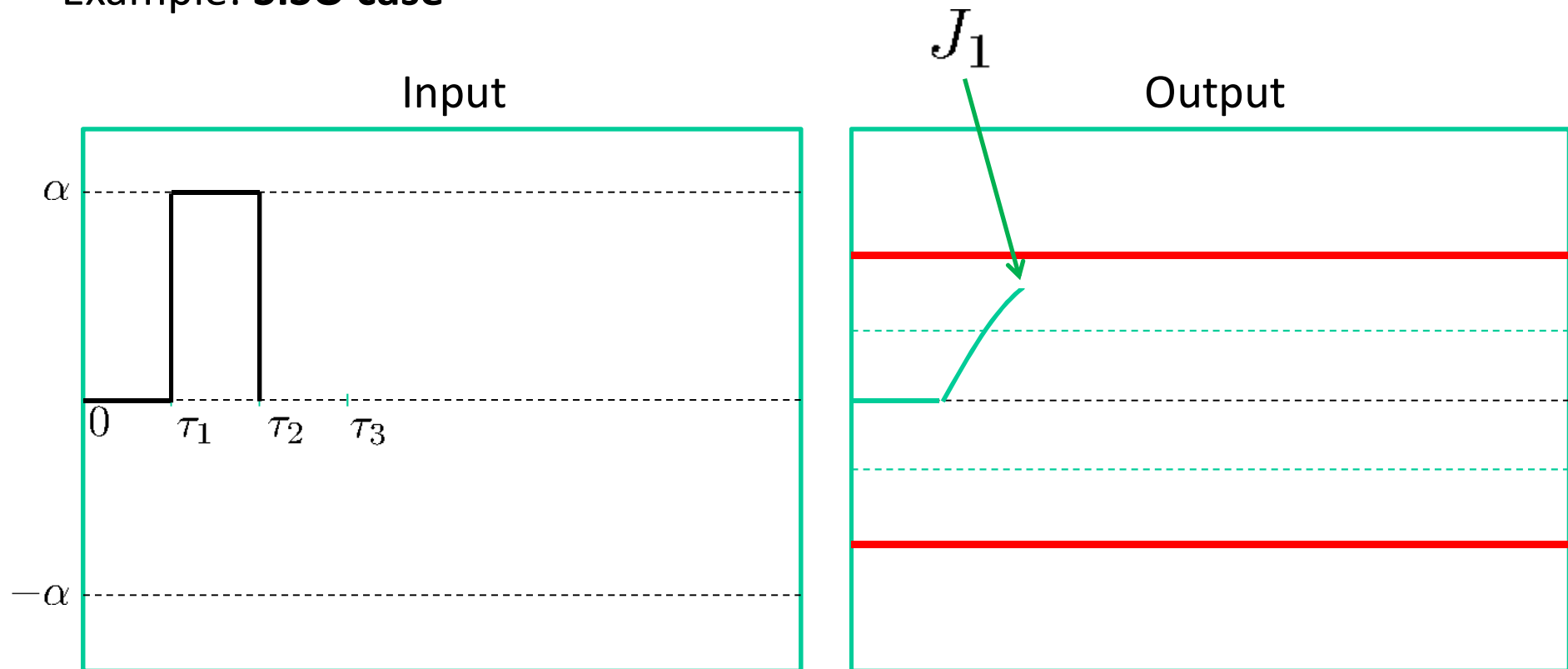
Example: **SISO** case





## Piecewise constant signals - 2

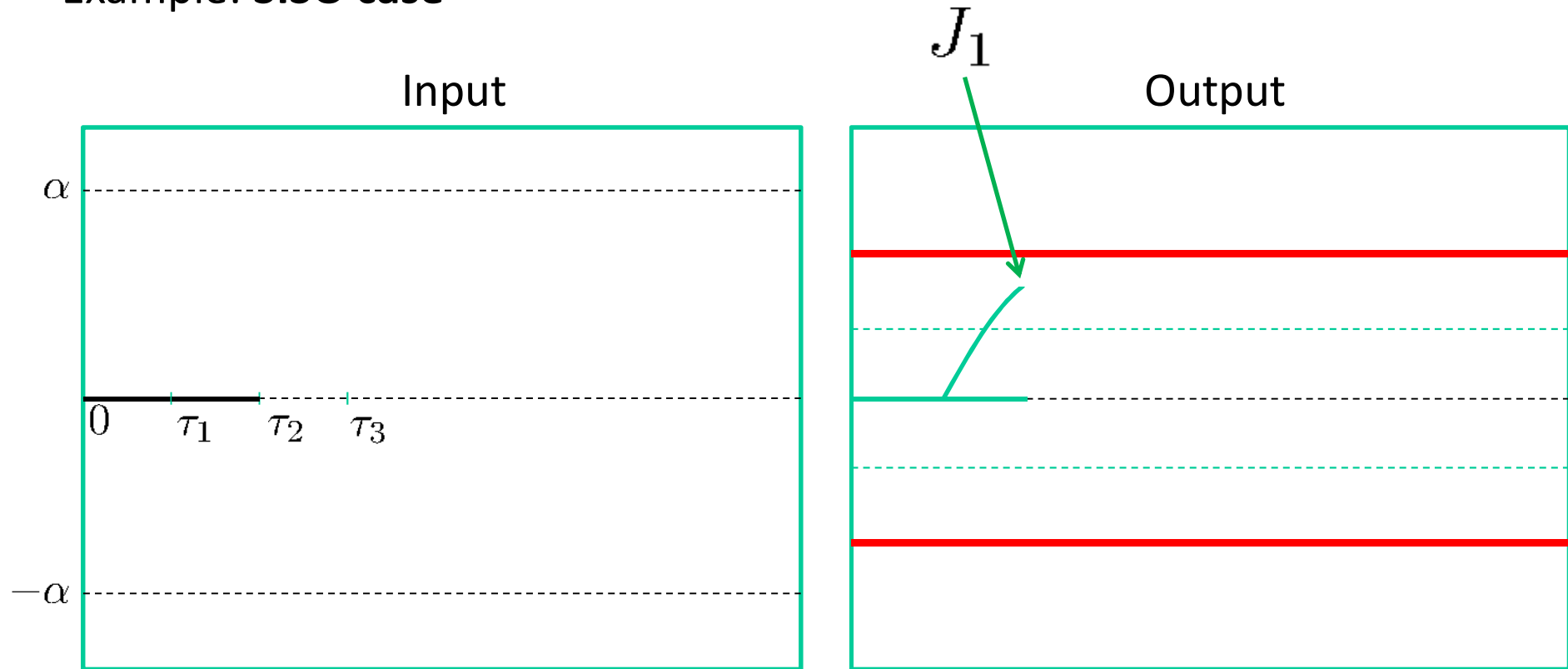
Example: **SISO** case





## Piecewise constant signals - 2

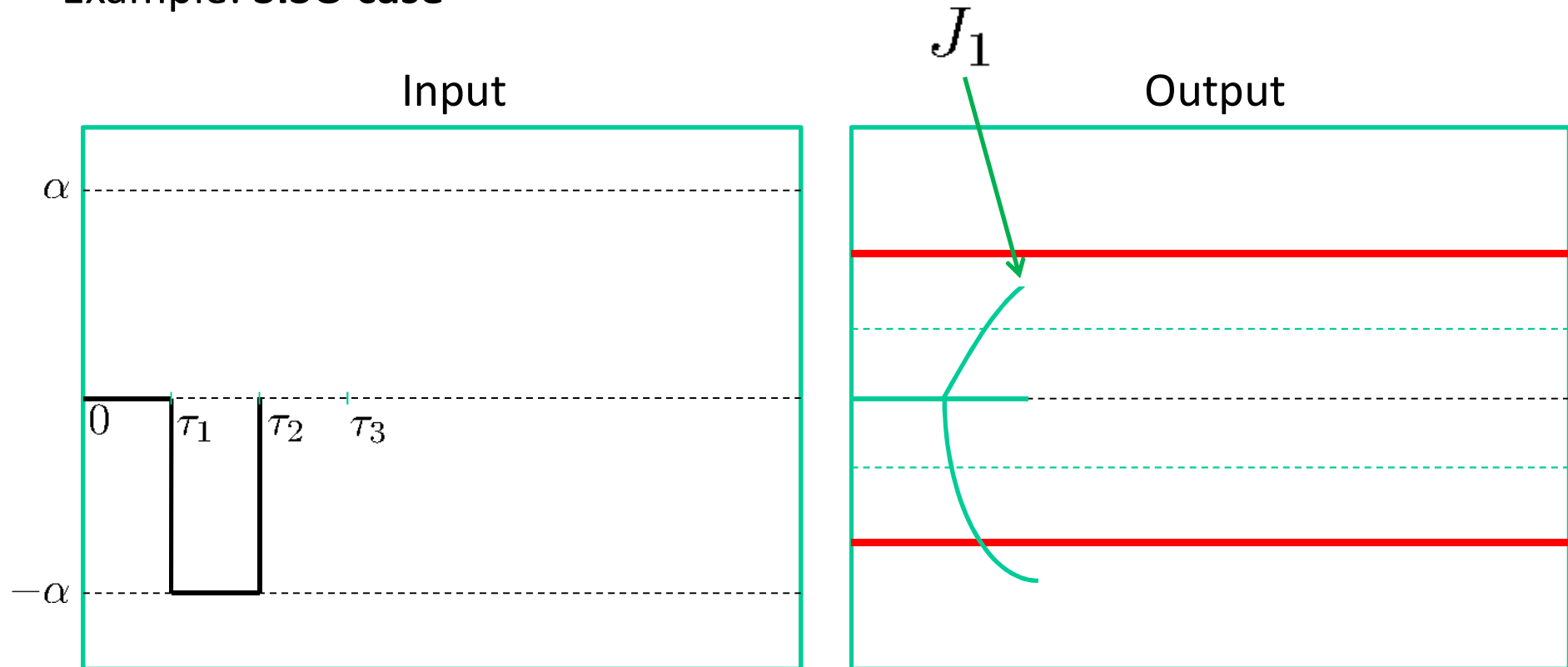
Example: **SISO** case





## Piecewise constant signals - 2

Example: **SISO** case

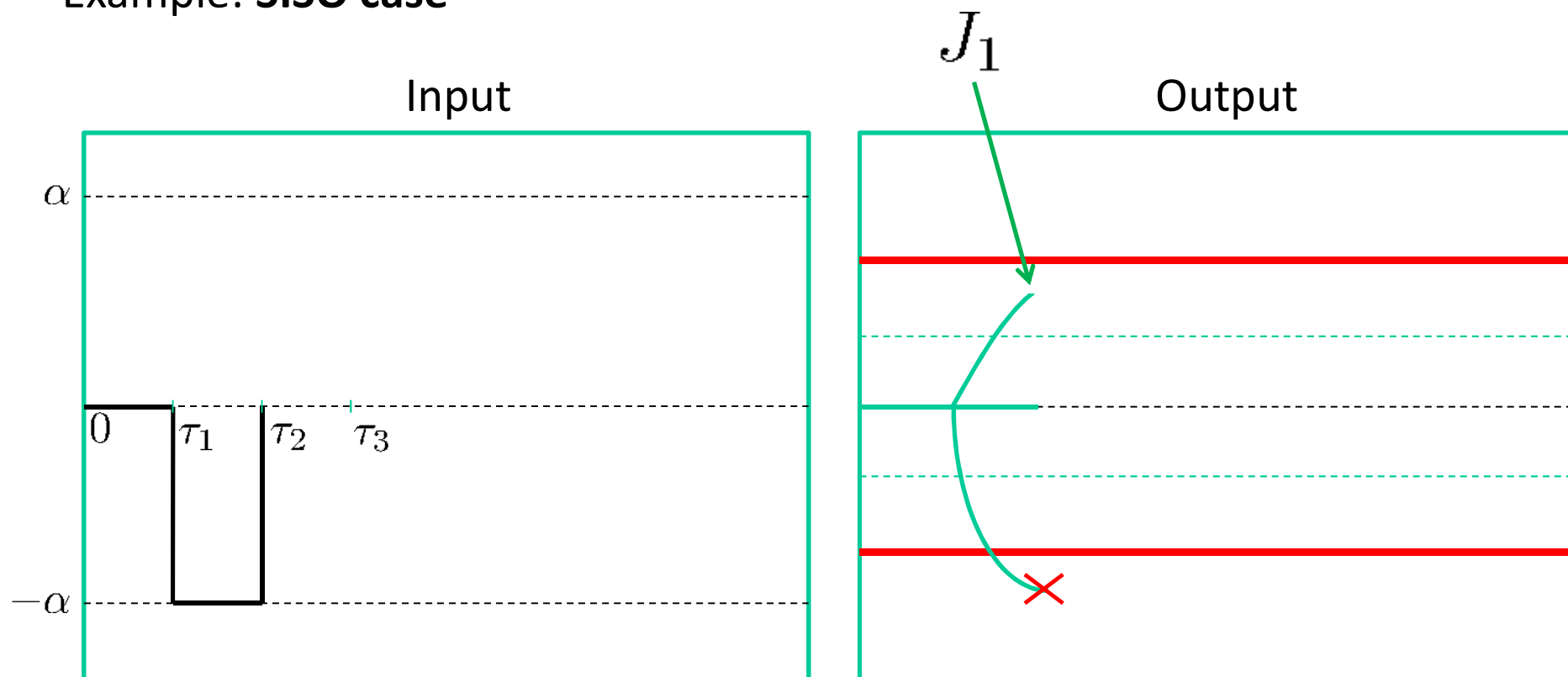






## Piecewise constant signals - 2

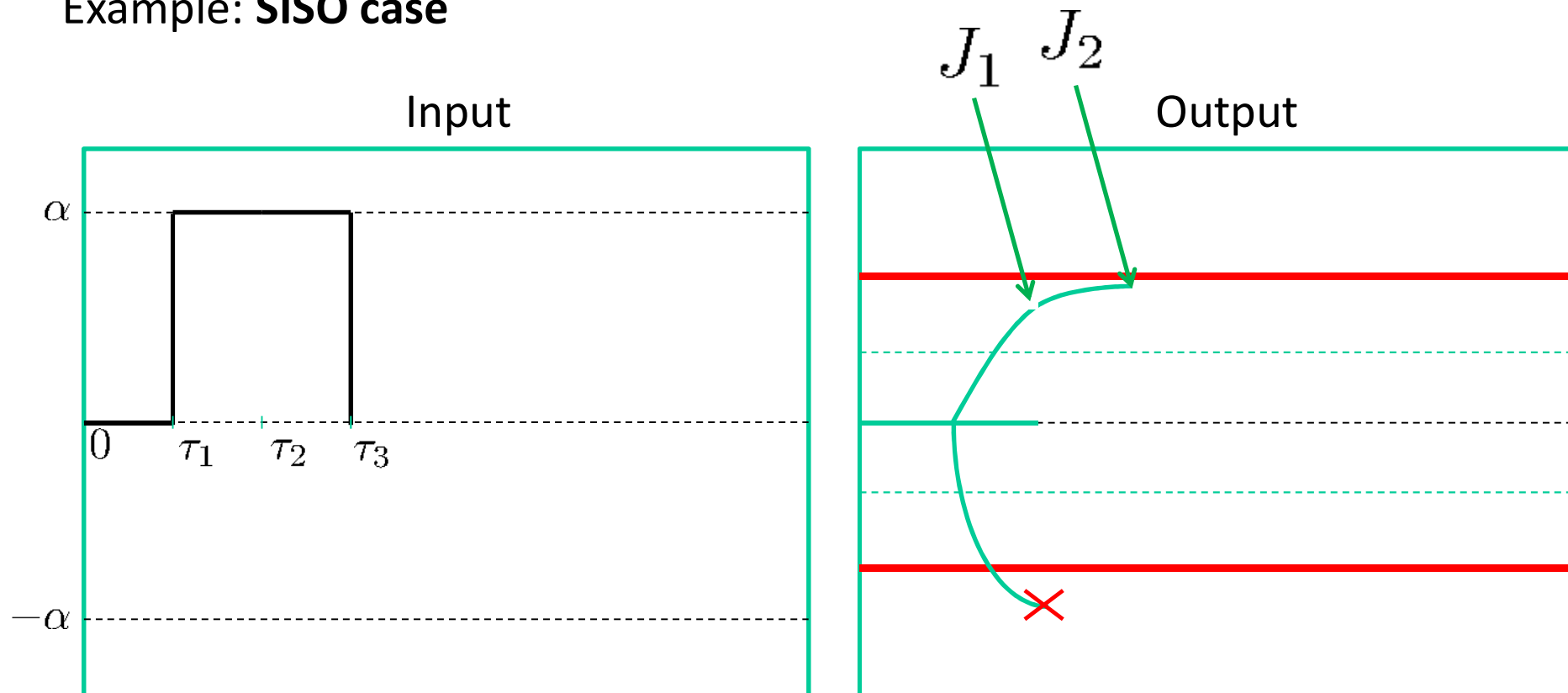
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## Piecewise constant signals - 2

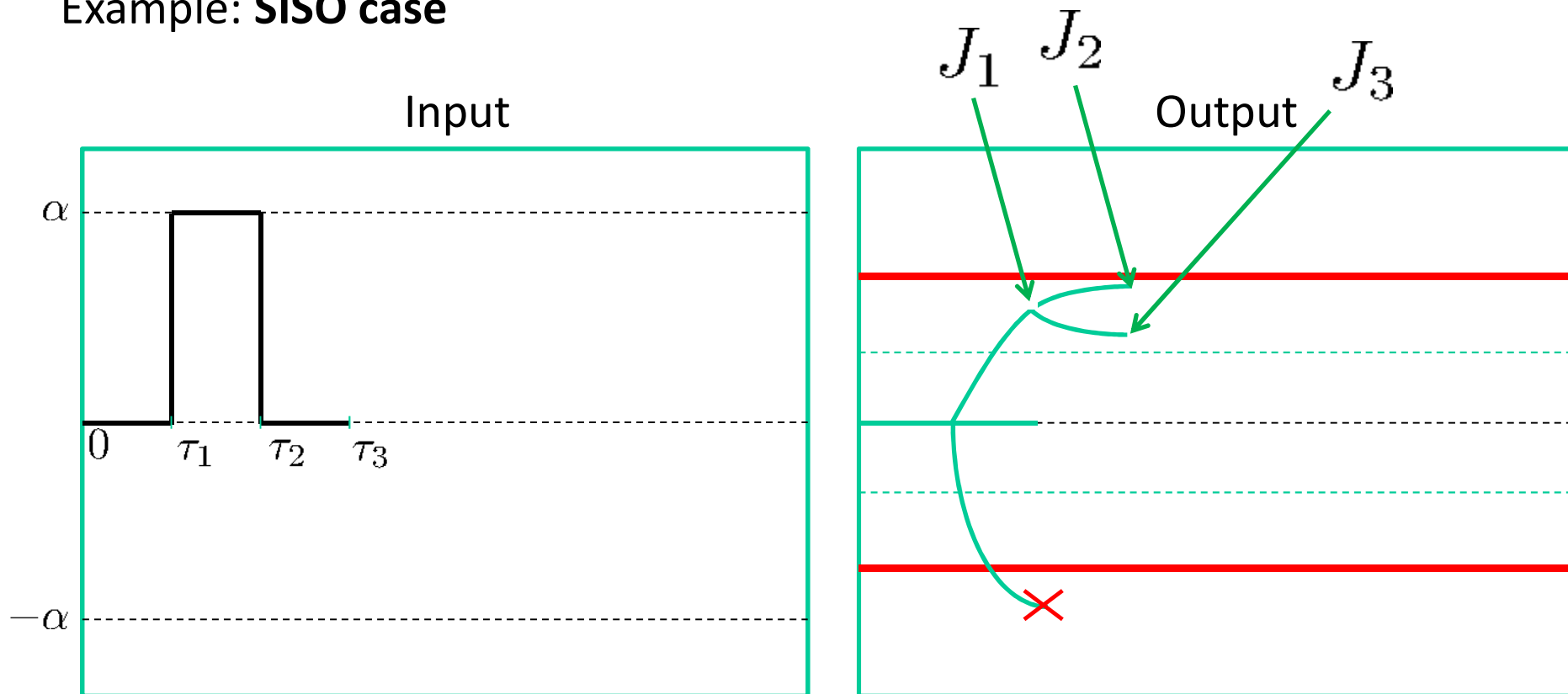
Example: **SISO** case





# Piecewise constant signals - 2

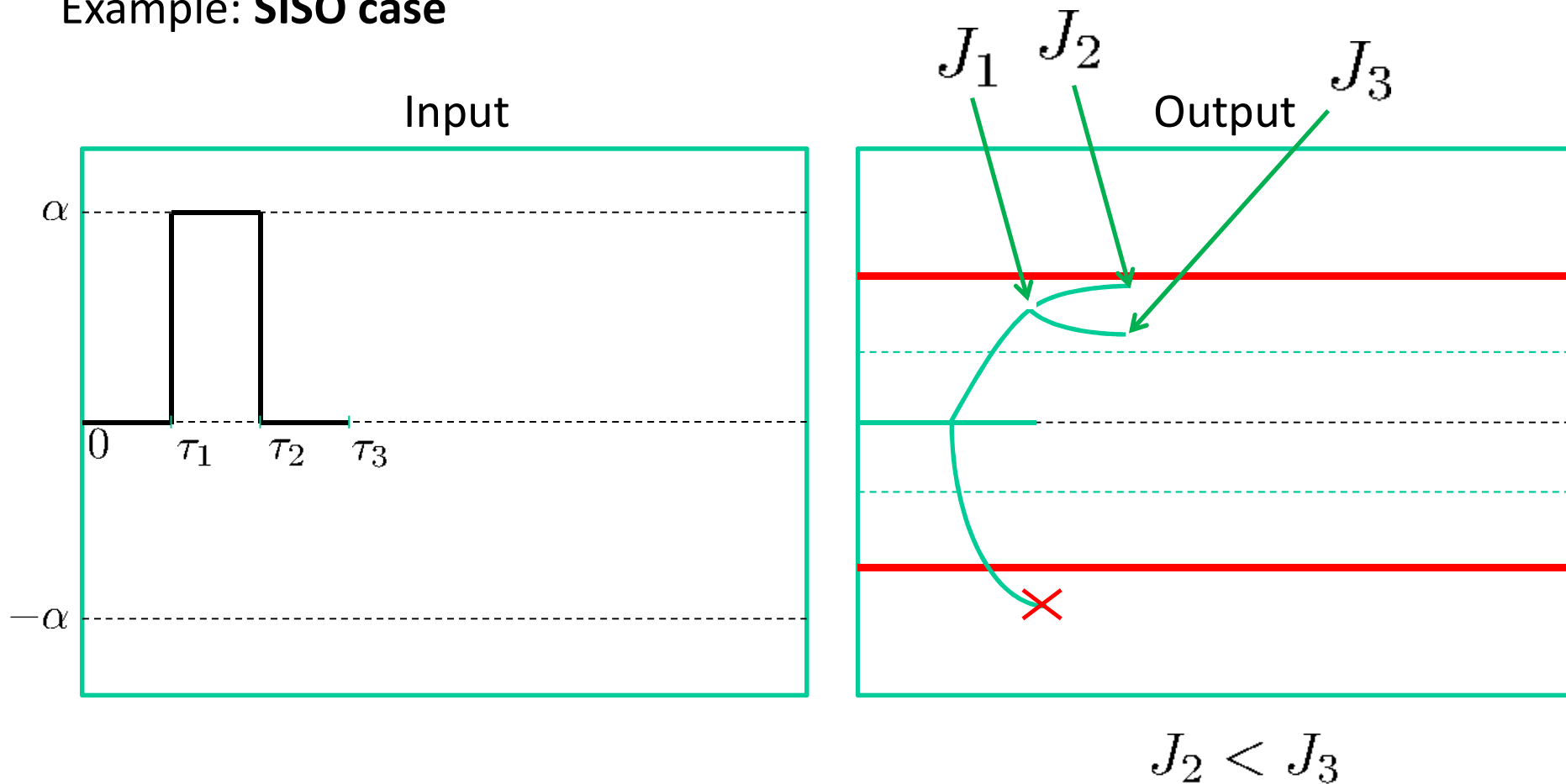
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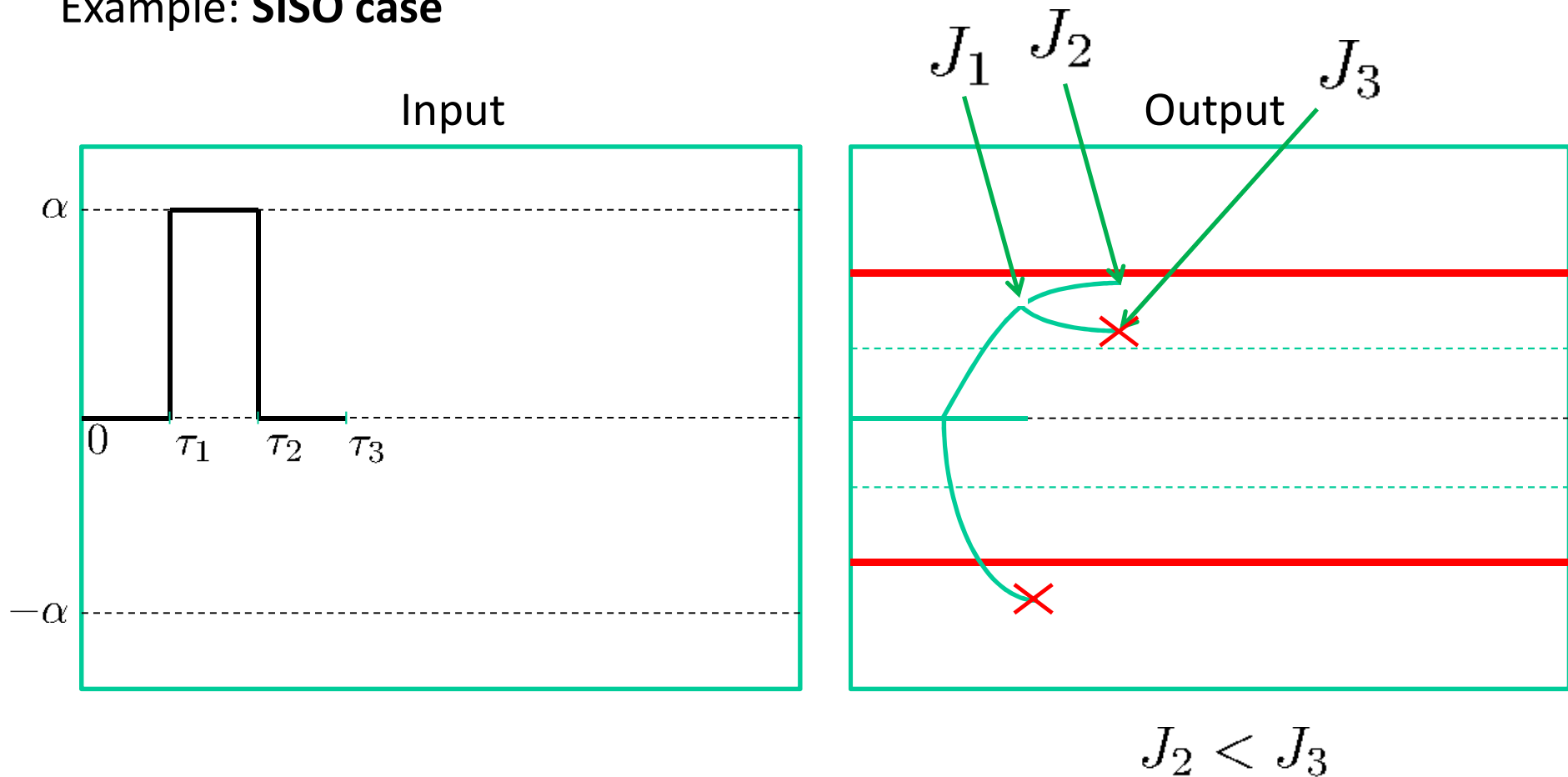
Example: **SISO** case





## Piecewise constant signals - 2

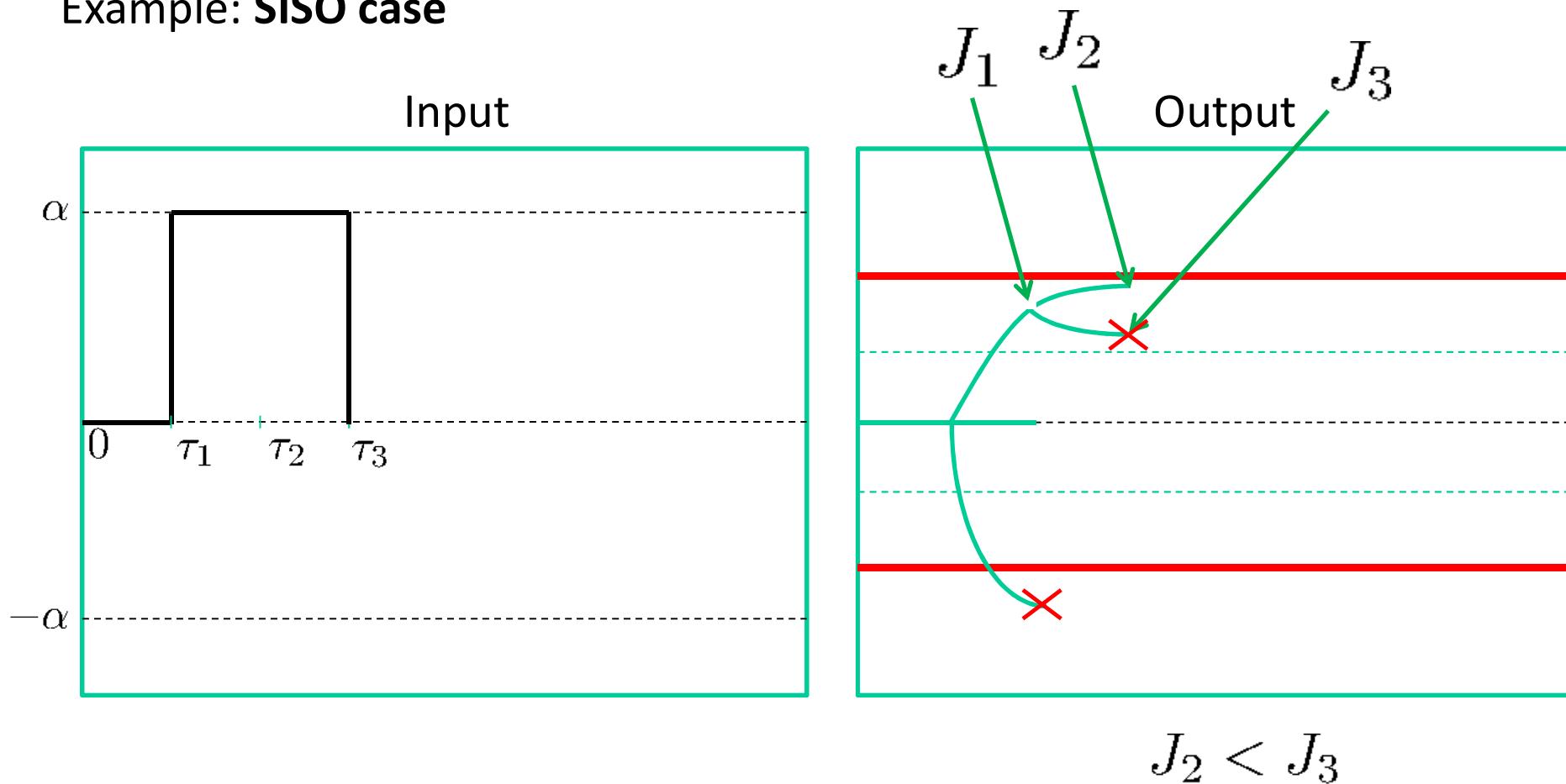
Example: **SISO** case





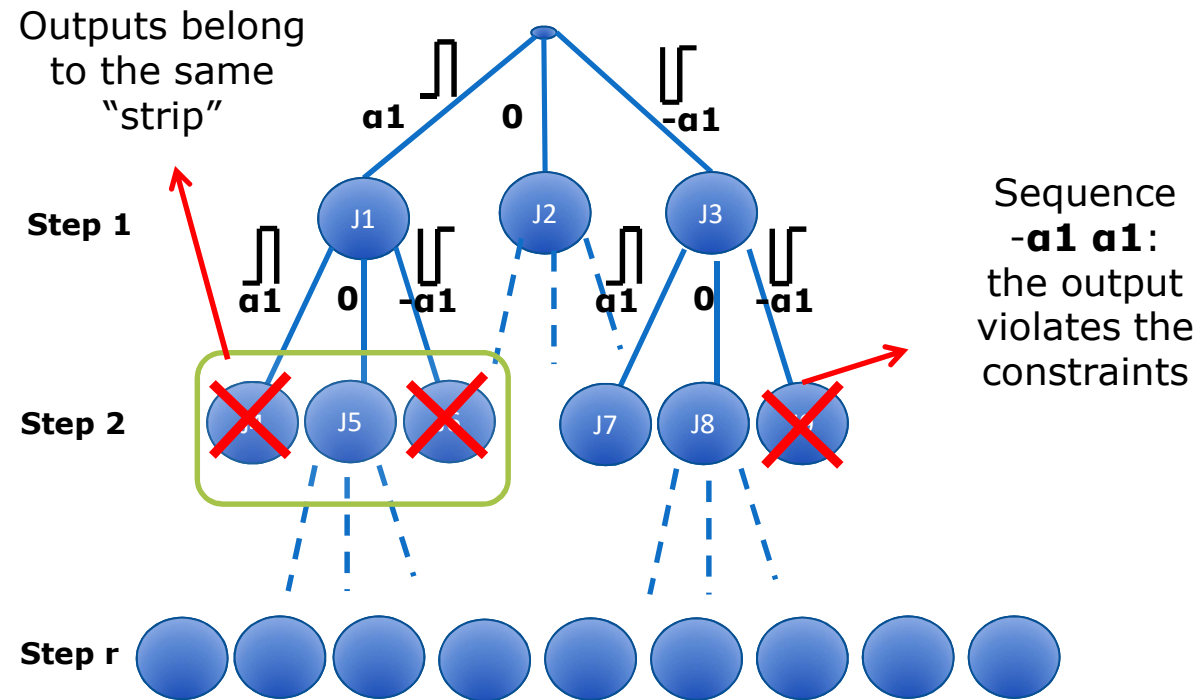
# Piecewise constant signals - 2

Example: **SISO** case





# Piecewise constant signals - 3





## Second step

Approximation of  $u(t)$

$$\tilde{u}(t) = \bar{u} + \sum_{k=1}^r \frac{a_k \bar{\varepsilon}_k - a_{k-1} \bar{\varepsilon}_{k-1}}{1 + e^{K(t_k - t)}}$$

## Initial solution

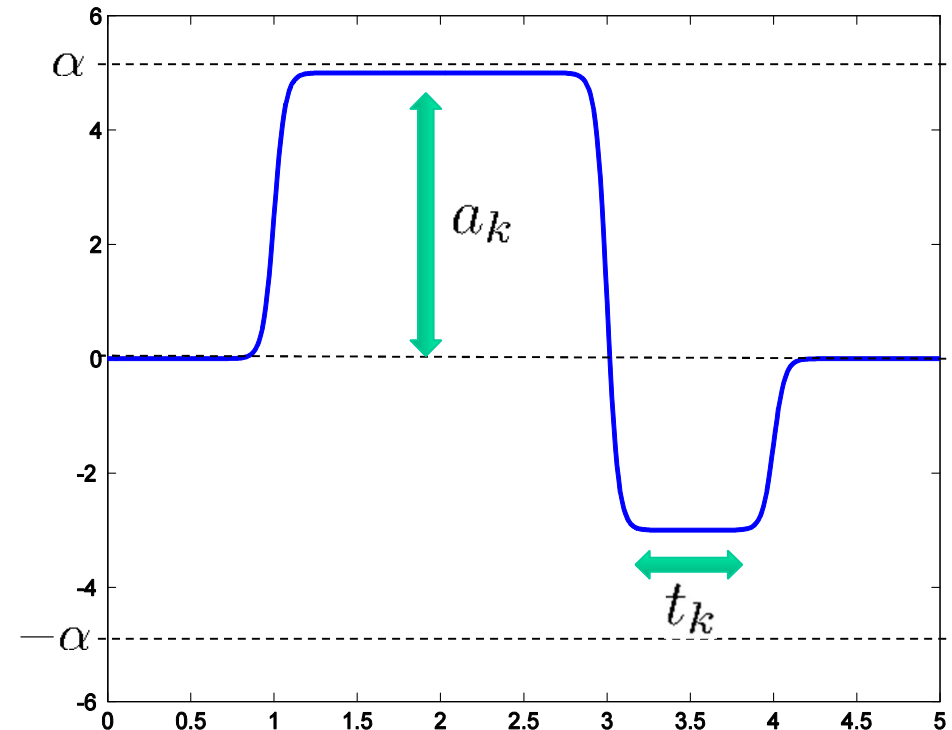
✓ First step Optimal solution

## Optimisation variables

- ✓ Duration of each step ( $t_k$ )
- ✓ Signal amplitude ( $a_k$ )

## Multiple input

✓ Input orthogonality  Time skew





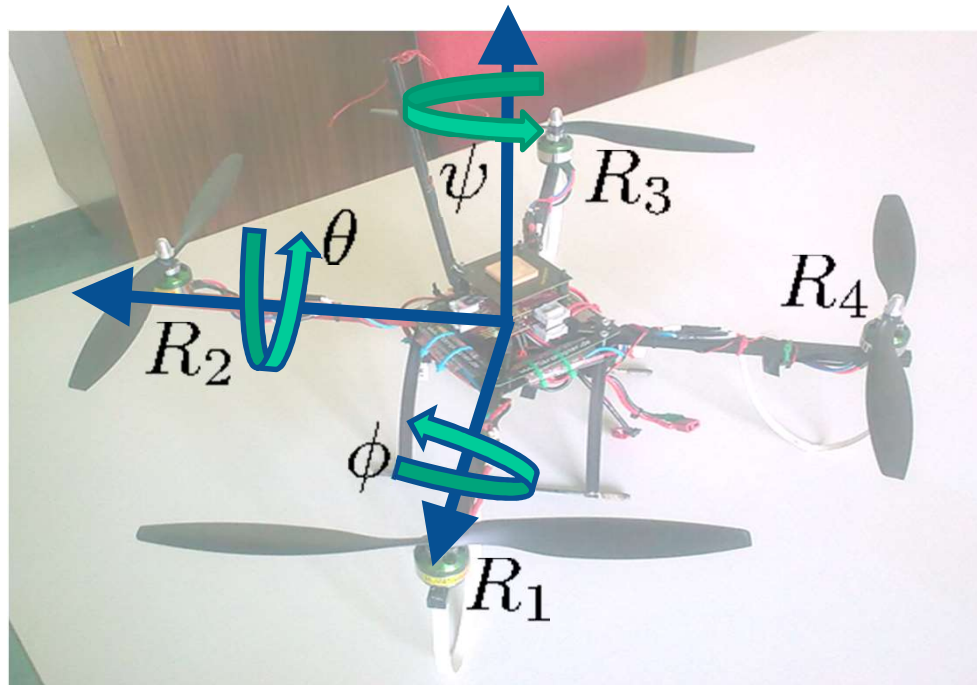


# Quadrotor UAV



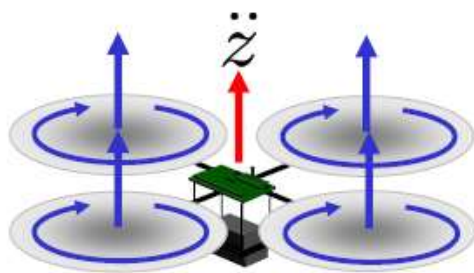


# Quadrotor UAV

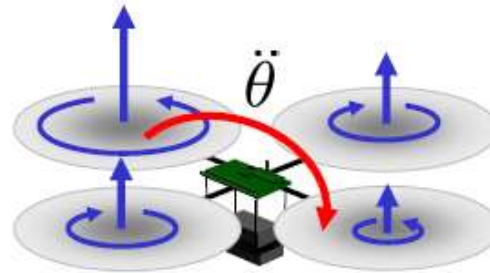


- ✓ 4 independent rotors
- ✓ Attitude control

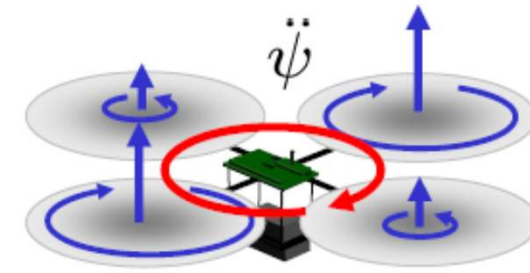
- ✓ Collective  
 $U_1 = \Omega_1^2 + \Omega_2^2 + \Omega_3^2 + \Omega_4^2$
- ✓ Roll  
 $U_2 = \Omega_4^2 - \Omega_2^2$
- ✓ Pitch  
 $U_3 = \Omega_3^2 - \Omega_1^2$
- ✓ Yaw  
 $U_4 = \Omega_2^2 + \Omega_4^2 - \Omega_1^2 - \Omega_3^2$



Collective



Pitch/Roll



Yaw



# Quadrotor model

4 inputs, 7 outputs

$$\dot{\phi} = p + \sin(\phi) \tan(\theta) q + \cos(\phi) \tan(\theta) r$$

$$\dot{\theta} = \cos(\phi) q - \sin(\phi) r$$

$$\dot{\psi} = \frac{\sin(\phi)}{\cos(\theta)} q + \frac{\cos(\phi)}{\cos(\theta)} r$$

$$\ddot{z} = -g + (\cos(\theta) \cos(\phi)) \frac{b}{m} U_1$$

$$\dot{p} = \frac{I_y - I_z}{I_x} q r + \frac{l b}{I_x} U_2$$

$$\dot{q} = \frac{I_z - I_x}{I_y} p r + \frac{l b}{I_y} U_3$$

$$\dot{r} = \frac{I_x - I_y}{I_z} p q + \frac{d}{I_z} U_4$$

## Model Parameters

Moments of Inertia

$$I_x \quad I_y \quad I_z$$

Aerodynamic coefficients

$$b \quad d$$



# Quadrotor model

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## Model Parameters

Moments of Inertia

$$I_x \quad I_y \quad I_z$$

Aerodynamic coefficients

$$b \quad d$$



# Quadrotor model

3 inputs, 7 outputs

$$\dot{\phi} = p + \sin(\phi) \tan(\theta) q + \cos(\phi) \tan(\theta) r$$

$$\dot{\theta} = \cos(\phi) q - \sin(\phi) r$$

$$\dot{\psi} = \frac{\sin(\phi)}{\cos(\theta)} q + \frac{\cos(\phi)}{\cos(\theta)} r$$

$$\ddot{z} = -g + (\cos(\theta) \cos(\phi)) \frac{b}{m} U_1$$

$$\dot{p} = \frac{I_y - I_z}{I_x} q r + \frac{l b}{I_x} U_2$$

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## Model Parameters

Moments of Inertia

$$I_x \quad I_y \quad I_z$$

Aerodynamic coefficients

$$\cancel{b} d$$



## Maneuver constraints

- ✓ Flight condition: **hover**
- ✓ Open-loop
- ✓ Unstable equilibrium
- ✓ Output constraints

$$|\phi| \leq 0.35 \text{ rad}$$

Roll

$$|\theta| \leq 0.35 \text{ rad}$$

Pitch

$$|\ddot{z}| \leq 1 \frac{m}{s^2}$$

Vertical Acceleration



## Results: optimal cost

Input signal class	Cost function ( $J=\text{Tr}[M^{-1}]$ )	
	Initial guess	Optimal solution
Multisine	$1.57 \times 10^{-4}$	$1.51 \times 10^{-6}$
Piece-wise constant	-----	$4.11 \times 10^{-7}$

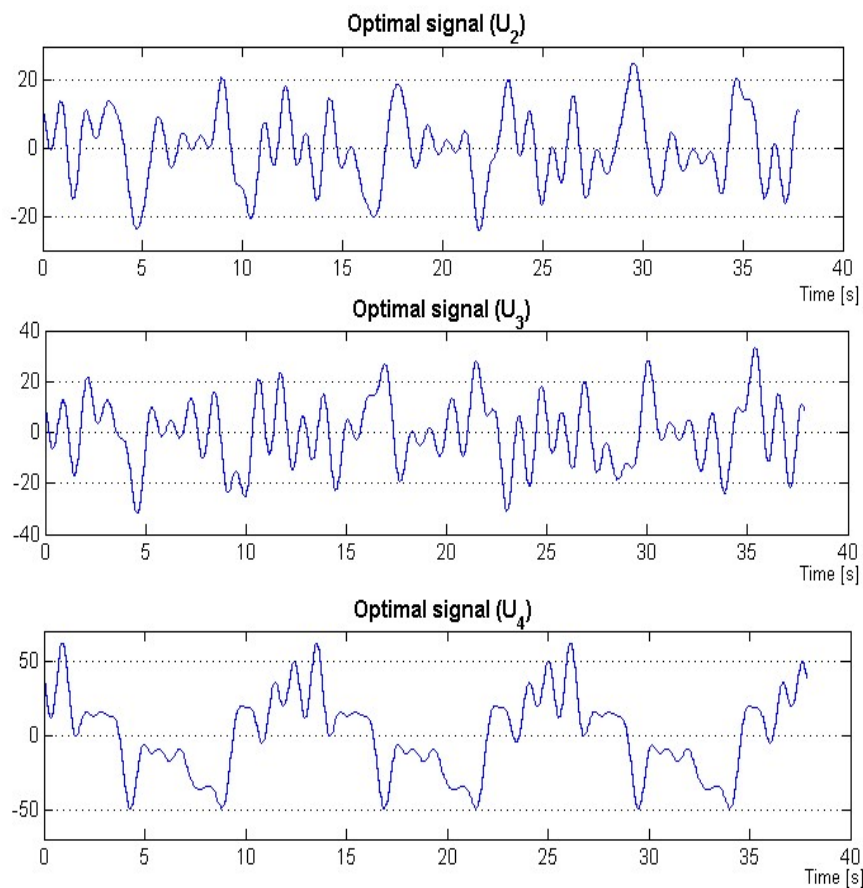


# Results: multisine signals

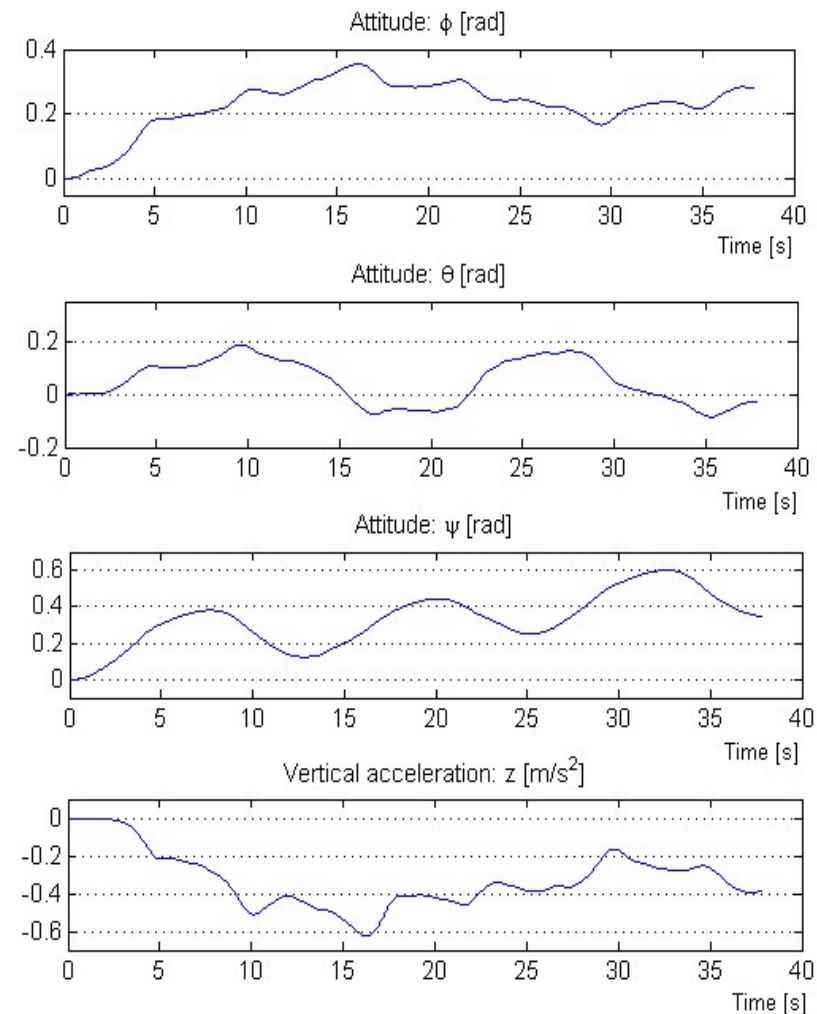
## Inputs

Experiment duration: 38 s

Bandwidth: 1 - 6 rad/s



## Outputs





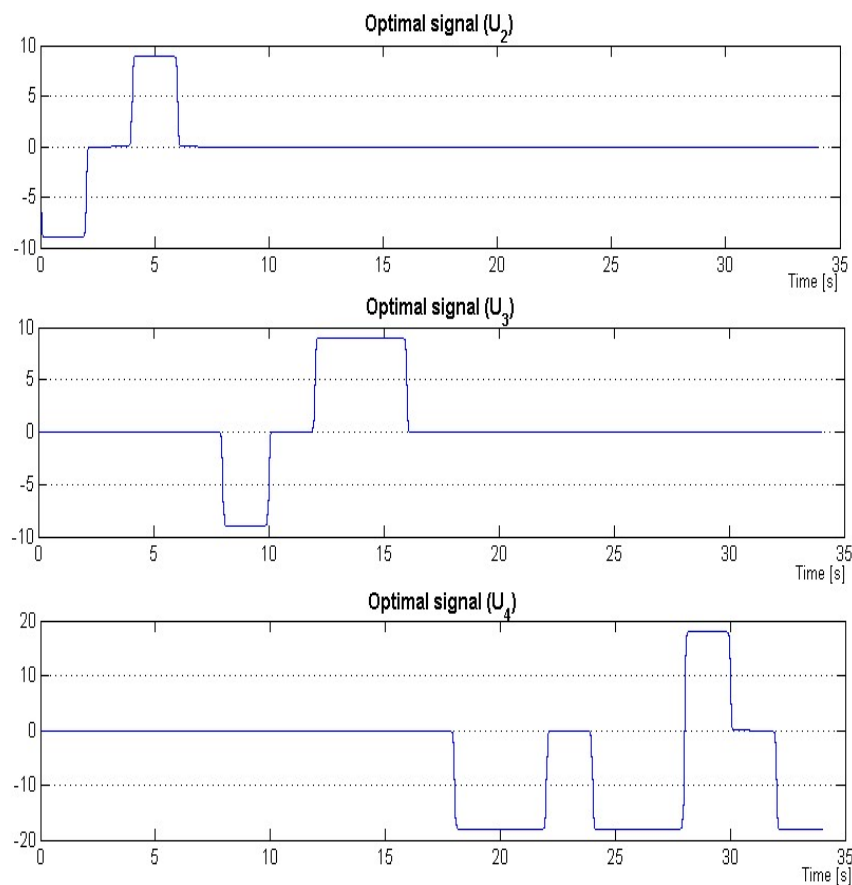


# Results: piecewise constant signals

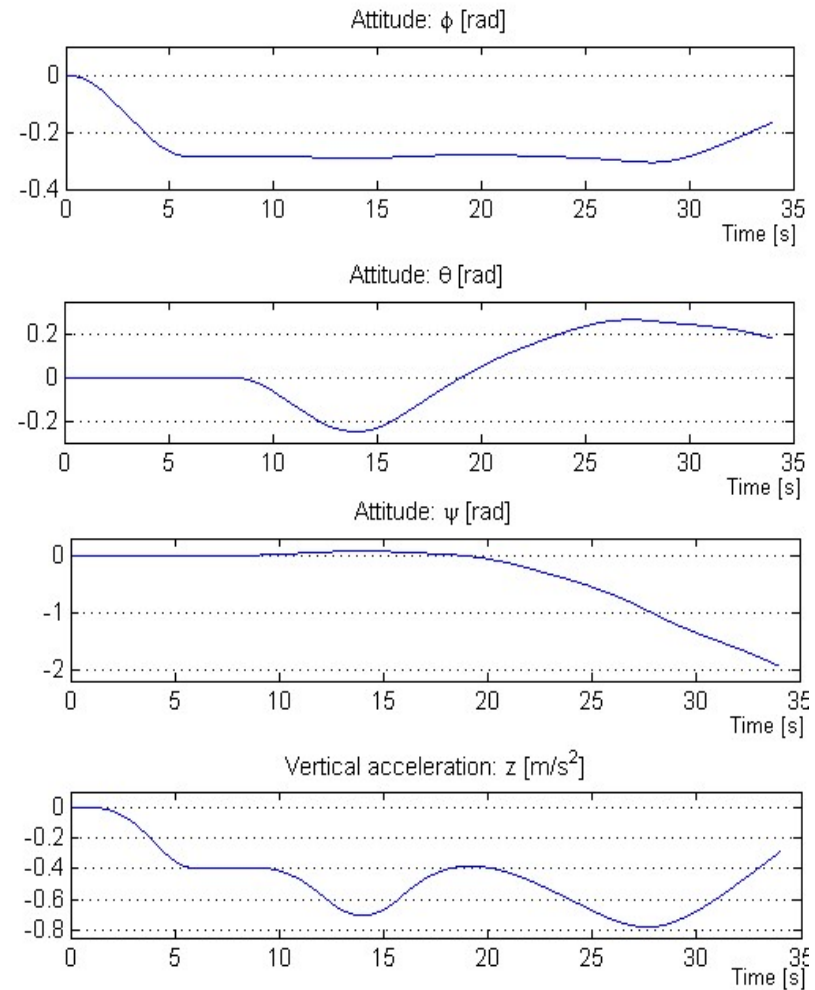
## Inputs

Experiment duration : 34 s

Steps: 17



## Outputs

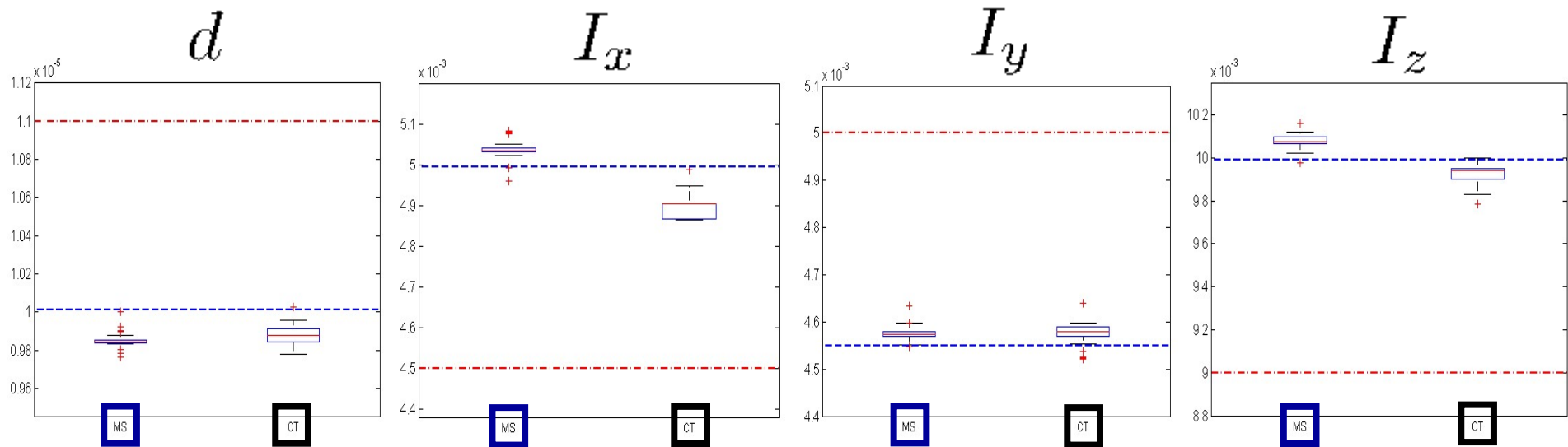




# Results: identification

- ✓ Output Error Method
- ✓ Output noise

- ✓ Initial error of the true value: 10%
- ✓ 50 runs



Initial value	---	Multisines	<input type="checkbox"/>
True value	---	Piecewise constant	<input type="checkbox"/>